

BOSTON REGION METROPOLITAN PLANNING ORGANIZATION

Stephanie Pollack, MassDOT Secretary and CEO and MPO Chairman Karl H. Quackenbush, Executive Director, MPO Staff

TECHNICAL MEMORANDUM

DATE: May 21, 2015

TO: Jeffrey Bina, Town Engineer, Westwood

FROM: Seth Asante, MPO Staff

RE: Safety and Operations Analyses—Westwood

Selected Intersections: High Street at Nahatan Street and High

Street at Pond Street in Westwood

This memorandum summarizes the analyses and improvement strategies for two intersections: High Street at Nahatan Street and High Street at Pond Street in Westwood. The opening sections give a background of the study and describe the existing conditions and problems that concern the community. Following that is an assessment of the safety and operations problems and a discussion of the potential improvement strategies. The final section of the memo presents the study recommendations. The memorandum also includes technical appendices that cite the methods used and data applied in the study, including detailed reports of the intersection capacity analyses.

1 BACKGROUND

In November 2013, the Town of Westwood submitted a list of intersections with safety and congestion issues to the Metropolitan Planning Organization (MPO) (Appendix A¹). The town wanted the MPO to consider these intersections when selecting various sites for Unified Planning Work Program (UPWP) studies, such as Safety and Operations Analyses at Selected Intersections—Federal Fiscal Year (FFY) 2014. In addition, the Town of Westwood expressed its intention to cooperate with and support the MPO in this planning study, and to implement the recommended improvements where appropriate, and based on the town's ability to fund them. The two intersections discussed here were chosen from the list for study under the Safety and Operations Analyses at Selected Intersections program.

_

¹ Appendix A includes a letter from Michael Jaillet, Town Administrator, Westwood to Karl Quackenbush, Executive Director, CTPS, dated November 12, 2013, which supports a study at the two intersections. This appendix also contains a list of task force members, and comments from Westwood and MassDOT—which have been addressed and incorporated in this memorandum.

The purpose of the Safety and Operations Analyses at Selected Intersections program is to identify problems at intersections in the region's arterial highways that experience many crashes, congestion, or mobility issues for buses, bicyclists, and pedestrians and develop multimodal solutions to address the problems identified. The MPO has been conducting these planning studies for the past ten years, and municipalities in the region are very receptive to them. The studies give towns the opportunity to look at the requirements of a specific location, starting at the conceptual level, before they commit funds for design and engineering. Moreover, if the project qualifies for federal funds, the study's documentation eventually would be useful to the Massachusetts Department of Transportation (MassDOT) as well.

Following a selection process,² four locations from a short list of 21 intersections were approved for study by the Boston Region MPO based on a series of criteria including, high crash rate, number of pedestrian and bicycle crashes, transit significance³, regional significance⁴, and implementation potential⁵. The four locations approved for study are:

- Washington Street (Route 53) and Broad Street in Weymouth
- Medway Road (Route109) at Kmart Shopping Plaza in Milford
- High Street (Route 109) at Nahatan Street in Westwood
- High Street (Route 109) and Pond Street in Westwood

The two Westwood locations were selected because of their safety and congestion problems (Figure 1).

1.1 Public Participation

An advisory task force composed of representatives from Westwood was established to participate in this study. MPO staff met with the task force two times: 1) to discuss the work scope and finalize existing conditions and problems, and 2) to present improvement concepts for comment. Working in conjunction with the task force, MPO staff collected data and conducted analyses to identify and quantify existing problems and their proposed improvement strategies. Both the task force and MassDOT Highway Division District 6 staff reviewed the study documents (Appendix A).

² Seth Asante, memorandum to Boston Region MPO, Safety and Operations Analyses at Selected Intersections—FFY 2013, Task 1: Intersection Selection Procedure, December 19, 2013.

³ Transit Significance: Location carries bus route(s) or is adjacent to a transit stop or station.

⁴ Regional Significance: Location carries high proportion of regional traffic or noticeable commuter bicycle traffic.

⁵ Implementation Potential: Location either is under MassDOT jurisdiction, has a Transportation Improvement Process (TIP) "conceptual" status, or has a strong commitment from a city or town.



FIGURE 1 Study Area Map Safety and Operations Analyses at Selected Intersections–FFY 2014

2 ROADWAY AND INTERSECTIONS

2.1 Roadway

Route 109/High Street

Route 109 is a predominantly two-lane, two-way arterial roadway that passes through eight communities from east to west: Dedham, Westwood, Dover, Walpole, Medfield, Millis, Medway, and Milford. Although Route 109 is a state-numbered route, it is locally controlled. The roadway is part of the National Highway System (NHS) program and is eligible for federal funds provided for the program. It is functionally classified as a principal arterial. In Westwood, the local name for Route 109 is High Street (henceforth, used throughout the memorandum). High Street—near the Nahatan Street intersection between Pond Street and Saint Margaret Mary Church—has 10- to 15-foot wide landscaped-curbed median and two 11-foot wide travel lanes in each direction (Figure 2). There are five- to six-foot continuous and connected sidewalks on both sides. The posted speed limit is 30 miles per hour (mph) on the segment of High Street near Nahatan Street, and 35 mph on the segment near Pond Street (close to the Sheehan School). The right-of-way is approximately 80 feet wide near the intersection of High Street with Nahatan Street.

Nahatan Street

Nahatan Street is a town-owned roadway functionally classified as an urban minor arterial. It is a two-lane, two-way roadway running in a north-south direction, generally with 11-foot wide travel lanes. A five-foot-wide continuous and connected sidewalk with a grass buffer is provided on the west side of Nahatan Street. The sidewalk on the east side of Nahatan Street has gaps; however, crosswalks have been provided at the breakpoints to connect to the sidewalk on the west side for continuity. The right-of-way generally varies between 40 and 50 feet but widens significantly to about 180 feet at the approach to High Street because of the presence of a median, traffic islands, and turn lanes to channel traffic through the intersection (Figure 2). The posted speed limit is 30 mph in both directions, although it is reduced to 20 mph when the Thurston Middle School is in session.

Pond Street

Pond Street is a town-owned roadway, functionally classified as an urban collector. Pond Street is a two-lane, two-way loop that intersects High Street at two locations: 1) about 200 feet west of Nahatan Street, and 2) about 1.1 miles west of Nahatan Street near the Sheehan School. Both intersections were included in this study. The right-of-way is approximately 50 feet wide and the land use is zoned residential.

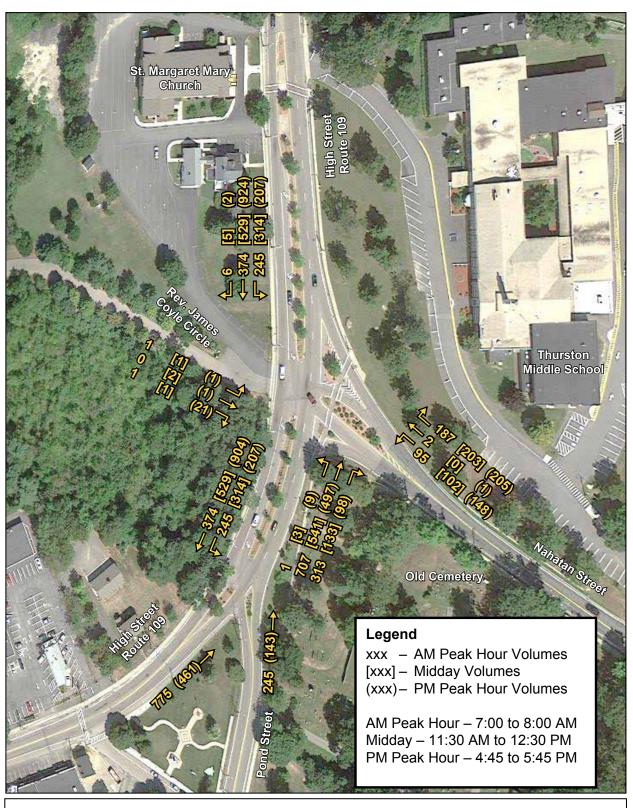


FIGURE 2

AM, Midday, and PM Peak Hour Traffic Volumes
High Street and Nahatan Street Intersection

Safety and Operations Analyses at Selected Intersections–FFY 2014 There is a five-foot continuous sidewalk with a grass buffer on one side of Pond Street. There are sidewalks on both sides of Pond Street near High Street, close to the Sheehan School.

The Reverend James W. Coyle Circle

The Reverend James W. Coyle Circle is a two-way driveway and access roadway, providing entry to Westwood New Cemetery and the Saint Margaret Mary Church. The roadway is not functionally classified and generally is used when there is a church or funeral activity.

2.2 Intersections

High Street and Nahatan Street

High Street, Nahatan Street, and Reverend James W. Coyle Circle form a four-legged two-way stop-sign-controlled intersection (Figure 2). The primary traffic flow through the intersection is along High Street. The intersection has multi-lane approaches because of high traffic volume during peak periods. The High Street eastbound approach widens to two lanes approximately 200 feet prior to the intersection and continues as two lanes through the intersection until approximately 300 feet past the intersection, where it merges into a single lane. The High Street westbound approach widens into two travel lanes approximately 250 feet prior to the intersection; the left approach lane is marked for left turns to Nahatan Street. The Nahatan Street northbound approach widens to accommodate two lanes: 1) a shared left/through lane controlled with a stop sign, and 2) an exclusive right-turn lane controlled with a yield sign.

The intersection has traffic islands and medians that channel traffic through the intersection and provide refuge for pedestrians crossing Nahatan Street. Sidewalks are present along all corners of the intersection, but only one crosswalk is provided at the intersection—for crossing Nahatan Street. The existing curb ramps do not meet ADA requirements—they lack detectable warning plates. The land use near the intersection is zoned residential. The Thurston Middle School is located in the northeast corner, the Saint Margaret Mary Church in northwest corner, and the Old Westwood Cemetery in the southeast corner of the intersection. Approximately 200 feet west of the Nahatan Street intersection is Pond Street, which intersects High Street to form a three-legged unsignalized intersection. Because of its close proximity, the Pond Street intersection was evaluated as part of analyzing the Nahatan Street intersection.

Pond Street and High Street (Near Sheehan School)

Pond Street and High Street form a three-legged unsignalized intersection (Figure 3). The primary traffic flow through the intersection is along High Street. The High Street eastbound approach widens to accommodate a free right turn



FIGURE 3 AM, Midday, and PM Peak Hour Traffic Volumes High Street and Pond Street Intersection

Safety and Operations Analyses at Selected Intersections—FFY 2014 onto Pond Street; but, the westbound approach is a single-lane approach. Traffic on Pond Street is controlled with a stop sign and drivers form two lanes at the approach during peak periods—one for turning left and one for turning right—because its approach is approximately 30 feet wide. The geometry of the intersection results in a long crosswalk on Pond Street. Curb ramps are present at the intersection but they lack detectable warning plates and do not meet ADA requirements.

3 VEHICLE, PEDESTRIAN, AND BICYCLE COUNTS

Traffic volume data were collected to assess operational characteristics of the intersections. MPO staff collected turning-movement counts (TMC) at the intersections in April 2014, when schools were in session (Appendix B). The counts were conducted during weekday morning, midday, and evening peak travel periods. All TMCs were conducted from 7:00 to 9:00 AM, 11:00 AM to 2:00 PM, and 3:00 to 6:00 PM. Heavy vehicles, including school buses, and trucks, were counted separately. Pedestrian and bicycle counts were conducted simultaneously with the TMCs.

Based on the counts, the average weekday traffic volume on High Street was approximately 20,200 vehicles per day (VPD) east of Nahatan Street; 9,300 VPD on Nahatan Street near High Street; and 7,400 VPD on Pond Street near the Sheehan School. Figures 2 and 3 show the turning movement volumes at the intersections. At both intersections, the primary High Street traffic flow (peak direction) is eastbound during the AM peak period and westbound on during the PM peak period. In addition, there are high-volume traffic interchanges between High Street and Nahatan Street, and between High Street and Pond Street (near the Sheehan School). The percentage of heavy vehicles observed at the intersections during the AM and PM peak periods, ranged between 3.0% and 5.5%. These rates are not considered particularly high for peak-period traffic conditions. In addition, staff did not detect any roadway geometry—such as turning radii, which would inhibit truck or bus traffic flow.

Table 1 presents the number of pedestrians and bicyclists observed at the two intersections during the eight-hour period when the TMCs were conducted. Students at the Thurston Middle School and neighborhood residents accounted for the majority of pedestrians observed at the intersection of High Street and Nahatan Street. At the High Street and Pond Street intersection, the majority of pedestrians were residents of that neighborhood.

TABLE 1
Number of Pedestrians and Bicyclists at the Study Intersections

Intersection	Pedestrian Count	Bicyclist Count
High Street at Nahatan Street	111	30
High Street at Pond Street (near Sheehan School)	23	23

Source: Central Transportation Planning Staff.

4 SAFETY CONDITIONS

4.1 Crash Summary

A summary of the crashes in terms of severity, manner of collision, ambient light, road surface, and weather conditions—based on 2009-2013 crash reports from the Westwood Police Department—is presented in Table 2. Records show 38 crashes at the High Street and Nahatan Street intersection during the five-year period. At the intersection of High Street and Pond Street (near the Sheehan School), records show nine crashes during the same period. The prevalent types of crashes at both intersections were rear-end and angle collisions. Records show one pedestrian crash at the crosswalk in front of the Saint Margaret Mary Church near the High Street and Nahatan Street intersection.

4.2 Crash Rates

Staff calculated intersection crash rates per the MassDOT Highway Division methodology, for the entire five-year period. The most recent statewide average crash rate for unsignalized intersections—based on MassDOT crash information queried on January 23, 2013—is 0.60 crashes per million entering vehicles (MEV). For MassDOT Highway Division District 6 (which includes the Town of Westwood), the average crash rate is 0.58 per MEV for unsignalized intersections. Analyses indicate that the average crash rate of 0.92 MEV for the High Street and Nahatan Street intersection exceeds the District 6 average crash rate for unsignalized intersections. The average crash rate of 0.26 MEV for the High Street and Pond Street intersection was below the District 6 average crash rate for unsignalized intersections. See Appendix C for crash rate work sheets.

4.3 Collision Diagram

MPO staff used police crash reports to prepare collision diagrams, which are useful for examining patterns and developing safety strategies (see Figures 4 and 5 below). The numbers in the collision diagram uniquely identify each crash and, for more detail about the crash, may be used to cross reference the crash records provided in Appendix C.

TABLE 2 Crash Summary (2009-2013)

	High Street and Nahatan	High Street and Pond Street
	Street and Pond Street	Intersection (near
Crash Variable	Intersection	Sheehan School)
Crash Severity		
Non-fatal injury	9	0
Property damage only	29	9
Manner of Collision		
Angle	9	8
Rear-end	16	0
Sideswipe, same direction	7	0
Single vehicle crash	6	1_
Road Surface Condition		
Dry	27	8
Wet	8	1
Snow	3	0
Ambient Light Conditions		
Daylight	27	7
Dark – lighted roadway	11	2
Weather Conditions		
Clear	25	5
Cloudy	4	3
Rain	6	1
Snow	3	0
Travel Period		
Peak-period	13	5
Off-peak	25	4
Total crashes	38	9
Five-year average (rounded)	8	2
Average crash rate	0.92	0.26
MassDOT Highway Division		
District 6 Crash Rate for	0.50	0.50
unsignalized intersection	0.58	0.58

^{*} The AM peak period is 7:00 AM to 9:00 AM, and the PM peak period is 4:00 PM to 6:00 PM. Source: Central Transportation Planning Staff.

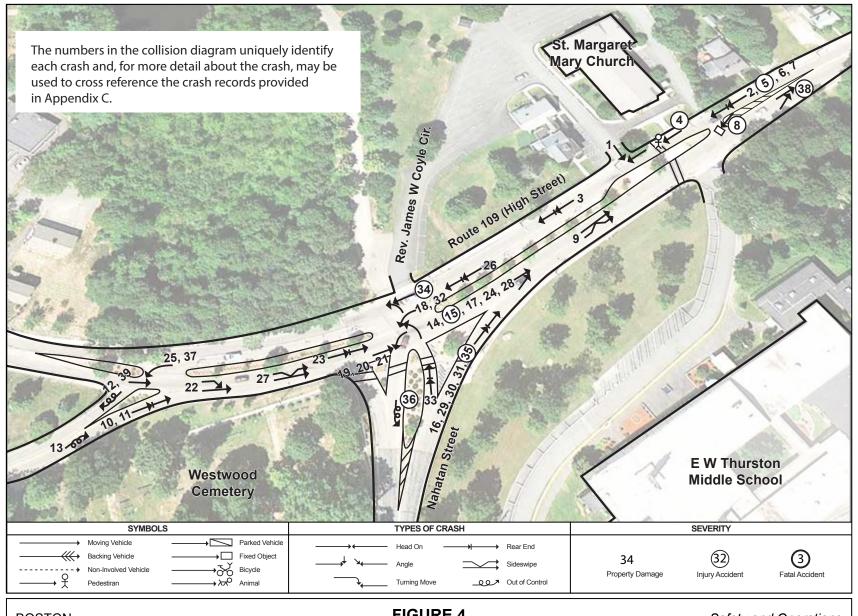


FIGURE 4
Collision Diagram for High Street and Nahatan Street Intersection (2009–2013)

Safety and Operations Analyses at Selected Intersections–FFY 2014

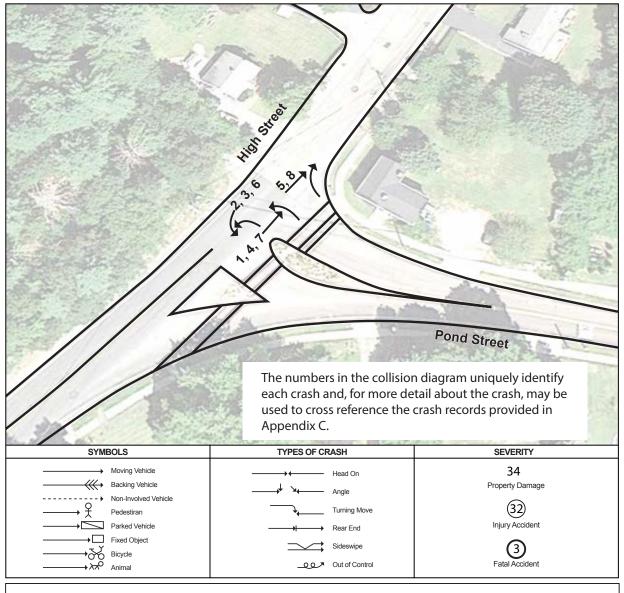


FIGURE 5
Collision Diagram for High Street and Pond Street Intersection (2009–2013)

Safety and Operations Analyses at Selected Intersections–FFY 2014 As seen in Figures 4 and 5 above, the prevalent crash patterns are:

- Angle type crashes involving High Street eastbound through movement and Nahatan Street right-turn movement (at merge point of the two movements (Figure 4)
- Rear-end type crashes involving Nahatan Street right-turn movement, near yield sign and crosswalk location (Figure 4)
- Angle type crashes involving High Street westbound left-turn movement and High Street eastbound through movement (Figure 4)
- Rear-end type crashes involving High Street westbound through movement near crosswalk connecting Thurston Middle School and Saint Margaret Mary Church (Figure 4)
- Angle type crashes involving Pond Street traffic entering High Street (Figure 5)

5 EXISTING TRAFFIC OPERATIONS CONDITIONS

Staff conducted traffic operations analyses consistent with the Highway Capacity Manual (HCM) methodologies (included in Appendix D)⁶. HCM methodology demonstrates driving conditions at signalized and unsignalized intersections in terms of level of service (LOS) ratings from A through F. LOS A represents the best operating conditions (little to no delay), while LOS F represents the worst operating conditions (very long delay). LOS E represents operating conditions at capacity (limit of acceptable delay). Table 3 presents the control delays associated with each LOS for unsignalized and signalized intersections. . Using the data collected, MPO staff built traffic analysis networks for the AM and PM peak hours with Synchro⁷ to assess the capacity and quality of traffic flow through the intersections.

TABLE 3
Intersection Levels of Service Criteria

interession Estate of Service Street							
Control Delay		Unsignalized Intersections Control Delay					
Level of Service	(seconds per vehicle)	(seconds per vehicle)					
A	0-10	0-10					
В	> 10-20	> 10-15					
С	> 20-35	> 15-25					
D	> 35-55	> 25-35					
E	> 55-80	> 35-50					
F	> 80	> 50					

Source: Highway Capacity Manual 2010.

6

⁶ Highway Capacity Manual 2010, Transportation Research Board of the National Academies, Washington, DC, December 2010.

⁷ Trafficware Inc., Synchro Studio 8, Synchro plus SimTraffic, Build 801, Version 563, Sugar Land, Texas.

Results of the peak-hour intersection capacity analyses (Table 4) indicate that traffic volumes on High Street are so large that drivers on Nahatan Street do not get adequate gaps to enter the intersection during peak hours—left-turn movements from Nahatan Street onto High Street operate at LOS F during peak hours. Staff observed similar traffic operations problems the High Street and Pond Street intersection during peak periods. Drivers turning left from Pond Street onto High Street experience much delay and operate at LOS F during peak hours—the 95th-percentile queue length range is 12-to-16 car lengths.

TABLE 4
Existing (2014) Peak-Hour Level of Service

Existing (2014) Peak-Hour Level of Service								
	Move	AM	AM	AM	PM	PM	PM	
Intersection / Approach	ment	LOS	Delay	Queue*	LOS	Delay	Queue	
High Street at Nahatan								
Street								
High St Eastbound	L+T+R	Α	0	0	Α	0	0	
High St Westbound	L	В	11.7	50	Α	9.4	25	
High St Westbound	T+R	Α	0	0	Α	0	0	
Rev. James Coyle Circle	L+T+R	D	32.4	25	D	30.6	25	
Nahatan St Northbound	L+T	F	97.5	150	F	92.8	150	
Nahatan St Northbound	R	В	14.5	50	В	11.1	25	
High Street at Pond Street								
(near Nahatan Street)								
High St Eastbound	Т	Α	0	0	Α	0	0	
High St Westbound	L	В	10.3	20	Α	9.6	50	
High St Westbound	Т	Α	0	0	Α	0	0	
Pond St Northbound	R	Е	35.5	125	В	13.5	50	
High Street at Pond Street							_	
(near Sheehan School)								
High St Eastbound	T+R	Α	0	0	Α	0	0	
High St Westbound	L+T	Α	0.6	0	Α	0.5	0	
Pond St Northbound	L	F	114.5	225	F	152.9	350	
Pond St Northbound	T+R	В	14.4	25	Α	9.8	5	

^a Delay in seconds per vehicle. ^b 95th percentile queue length in feet. # = the 95th-percentile volume exceeds capacity.

6 TRAFFIC SIGNAL WARRANT ANALYSIS

Traffic control signals are valuable devices for controlling vehicular and pedestrian traffic. They assign the right-of-way to various traffic movements and thereby strongly influence traffic flow. Traffic control signals that are properly designed, located, operated, and maintained will provide orderly movement of traffic, and reduce congestion and the frequency and severity of certain types of crashes, especially right-angle collisions. Traffic control signals are not solutions to all traffic problems at intersections. Poorly designed and maintained, ineffectively placed, improperly operated, or unjustified traffic control signals can

Source: Central Transportation Planning Staff.

result in excessive delays, significant increase in crashes (especially rear-end type), and diversion of traffic to less adequate routes, as road users attempt to avoid the traffic control signals. Investigating the need for a traffic control signal at an unsignalized intersection includes analyzing factors related to the existing operations and safety, as well as the potential to improve these conditions. Such an investigation is called traffic signal warrant analysis.

Using the methodology in the 2009 edition of Manual on Uniform Traffic and Control Devices⁸ (MUTCD), staff performed detailed traffic signal warrant analyses to determine whether installation of traffic control signals at the intersections is justified and if they would improve safety and traffic operations. The MUTCD lists nine traffic signal warrants that justify installing a traffic signal at a study location:

- Warrant 1, Eight-Hour Vehicular Volume
- Warrant 2, Four-Hour Vehicular Volume
- Warrant 3, Peak Hour
- Warrant 4, Pedestrian Volume
- Warrant 5, School Crossing
- Warrant 6, Coordinated Signal System
- Warrant 7, Crash Experience
- Warrant 8, Roadway Network
- Warrant 9, Intersection Near a Grade Crossing

Table 5 presents the results of the signal warrant analysis; detailed traffic signal warrant analysis worksheets are included in Appendix D. Existing conditions at High Street and Nahatan Street satisfy five of the warrants. Existing conditions at

TABLE 5
Results of Traffic Signal Warrant Analysis

Movement	High Street and Nahatan Street	High Street and Pond Street
Warrant	Intersection	Intersection
Warrant 1, Eight-Hour Vehicular Volume	Satisfied	Not satisfied
Warrant 2, Four-Hour Vehicular Volume	Satisfied	Satisfied
Warrant 3, Peak Hour	Satisfied	Satisfied
Warrant 4, Pedestrian Volume	Not satisfied	Not satisfied
Warrant 5, School Crossing	Not satisfied	Not satisfied
Warrant 6, Coordinated Signal System	Not satisfied	Not satisfied
Warrant 7, Crash Experience	Satisfied	Not satisfied
Warrant 8, Roadway Network	Satisfied	Satisfied
Warrant 9, Intersection Near a Grade Crossing	Not satisfied	Not satisfied

Source: Central Transportation Planning Staff.

_

⁸ US Department of Transportation, Federal Highway Administration, Manual on Uniform Traffic Control Devices for State Streets and Highways, 2009 Edition.

High Street and Pond Street satisfy three of the warrants. The MUTCD states that satisfying traffic signal warrants alone does not require installing a traffic control signal. The intersection of High Street and Pond Street did not satisfy the major warrants, Warrants 1 and 7. Warrant 1 is for locations with a large amount of intersecting traffic or where traffic on a major street is so heavy that, as a result, traffic on a minor intersecting street suffers excessive delay. Warrant 7 is for locations with frequent and severe crashes.

7 FUTURE CONDITIONS

To forecast systematically future traffic volume based on changes in the transportation network or land use, planners generally employ a planning model. For this study, staff utilized the Boston Region MPO's "regional travel demand model set" most recently adopted for its Long-Range Transportation Plan (LRTP). This model's socioeconomic components are derived from forecasts produced by the Metropolitan Area Planning Council (MAPC). The model is calibrated at a regional level for 164 cities and towns, which includes all of the 101 cities and towns in the MPO region. For site-specific development and transportation projects, the model needs to be calibrated to replicate local travel patterns in the project area before it may be used to forecast the project's future impacts. Using this model, staff projected that traffic on High Street would grow 0.3% per year, resulting in 3% total growth between 2014 and 2024.

8 IMPROVEMENTS

MPO staff developed and analyzed short- and long-term improvements to address the problems. Staff used the projected growth factors from the regional model set to expand existing peak-hour turning-movement volumes, which were used to test the improvement strategies. The results are included in Appendix D.

8.1 High Street and Nahatan Street Intersection

The concerns at the intersections are:

- Safety of pedestrians crossing at the intersection
- Drivers turning right from Nahatan Street onto High Street drive at high speeds because of a wide curb radius; are involved in many angle and rear-end crashes
- Limited sight distance for drivers turning right from Nahatan Street and merging onto High Street
- Merging and weaving traffic at the High Street eastbound approach

Below are the improvement strategies that staff evaluated for the intersection:

- Alternative 1: Replace the yield sign with a stop sign (short-term)
- Alternative 2: Install a pedestrian flashing beacon for crossing High Street at Saint Margaret Mary Church (short-term)
- Alternative 3: Reconfigure High Street eastbound approach lanes; tighten approach curb radius for Nahatan Street right-turn lane; add a stop sign (medium-term)
- Alternative 4: Tighten approach curb radius for Nahatan Street right-turn lane; add a stop sign (medium-term)
- Alternative 5: Install new traffic signal (long-term)
- Alternative 6: Construct a modern roundabout (long-term)

Short-Term Improvements

Alternative 1: Replace the yield sign (R1-2) on Nahatan Street with a stop sign (R1-1) and provide clear markings

The objective of Alternative 1 is to allow drivers to stop and look for adequate gaps to enter High Street. This strategy may be enhanced with targeted enforcement to reduce stop violations and supplementary pavement markings.



R1-2 Yield sign

The improvement would:

- Reduce angle crashes involving Nahatan Street right-turn movements and High Street eastbound through traffic movements
- Reduce rear-end crashes involving Nahatan Street right-turn movements



R1-1 Stop sign

Source: MUTCD 2009 edition

The improvement would not reduce traffic delays for Nahatan Street left-turn movements (Table 6).

The Federal Highway Administration⁹ estimates converting yield-sign control to stop-sign control could reduce related crashes between 9-and-29 percent. The cost of implementing these improvements, including signs and pavement markings, would cost less than \$5,000.

Alternative 2: Install a Pedestrian-Activated Flashing Beacon for the Crossing on High Street at Saint Margaret Mary Church

MPO staff proposes that a pedestrian-activated flashing beacon be installed for the marked crossing on High Street in front of Saint Margaret Mary Church and Thurston Middle School to give advance warning to drivers or pedestrians

⁹ Crash Modification Factors Clearinghouse, US Department of Transportation Federal Highway Administration.

TABLE 6
High Street and Nahatan Street Intersection Future Year (2024)
Peak-Hour Level of Service

Peak-Hour Level of Service								
	Move	AM	AM	AM	PM	PM	PM	
Improvement Alternative	ment	LOS	Delay ^a	Queue ^b	LOS	Delay	Queue	
Alternative 1: Stop Control								
High St Eastbound	L+T+R	Α	0	0	Α	0	0	
High St Westbound	L	В	12.2	50	Α	9.6	25	
High St Westbound	T+R	Α	0	0	Α	0	0	
Rev. James Coyle Circle	L+T+R	Ε	40.2	25	D	32.6	25	
Nahatan St Northbound	L+T	F	123	175	F	>180	300	
Nahatan St Northbound	R	С	15.1	50	В	12.3	25	
Total intersection	All	В	11.2		E	41.4		
Alternative 3: Reconfigure Lanes								
and Tighten Curb Radius								
High St Eastbound	L+T	Α	0	0	Α	0	0	
High St Eastbound	R	Α	0	0	Α	0	0	
High St Westbound	L	В	11.9	50	Α	9.8	25	
High St Westbound	T+R	Α	0	0	Α	0	0	
Rev. James Coyle Circle	L+T+R	Е	37.9	25	D	34.9	25	
Nahatan St Northbound	L+T	F	106.1	125	F	>180	300	
Nahatan St Northbound	R	Α	0	75	Α	Α	0	
Total Intersection	All	Α	7.7		Ε	46.1		
Alternative 4: Tighten Approach								
Curb Radius for Nahatan Street								
High St Eastbound	L+T+R	Α	0	0	Α	0	0	
High St Westbound	L	В	12.2	50	Α	9.6	25	
High St Westbound	T+R	Α	0	0	Α	0	0	
Rev. James Coyle Circle	L+T+R	Е	40.2	25	D	32.6	25	
Nahatan St Northbound	L+T	F	123	175	F	>180	300	
Nahatan St Northbound	R	С	15.1	50	В	12.3	25	
Total Intersection	All	В	11.2		Е	41.4		
Alternative 5: Traffic Signal								
High St Eastbound	L+T+R	С	21.6	#536	В	18.8	227	
High St Westbound	L	С	32.2	#308	В	12.6	124	
High St Westbound	T+R	Α	8.3	251	С	26.9	#933	
Rev. James Coyle Cir	L+T+R	С	27	12	С	26.6	12	
Nahatan St Northbound	L+T	D	43.4	130	D	43	#191	
Nahatan St Northbound	R	С	22.2	114	С	16.4	98	
Total Intersection	All	С	21.5		С	23.3		
Alternative 6: Roundabout								
High St Eastbound	L+T	Е	45.1	0	D	29.7	215	
High St Eastbound	R	Α	0		Α	0	0	
High St Westbound	L+T+R	Α	7.6	0	С	15.9	150	
Rev. James Coyle Cir	L+T+R	Α	7.7	25	В	14.2	25	
Nahatan St Northbound	L+T	C	16.2	130	Ā	9.4	25	
Nahatan St Northbound	R	Ā	0	50	A	0.1	25	
Total Intersection	AII	C	19.8		C	16.5		
	, , , , ,					. 0.0		

^a Delay in seconds per vehicle. ^b 95th percentile queue length in feet. # = the 95th percentile volume exceeds capacity. Source: Central Transportation Planning Staff.

crossing High Street. During 2009-2013, there was one pedestrian-vehicle collision in the crosswalk and four rearend crashes near crosswalk. According to the MUTCD, warning beacons that are actuated by pedestrians, bicyclists, or other road users may be used to provide additional warning to vehicles approaching a crossing. Pedestrian flashing beacons should be accompanied by pedestrian warning sign W11-2 or school crossing sign S1-1 and W16-7p.

Research indicates that going from a no-beacon to a beacon system—mounted on supplementary warning signs on the right and left sides of the crossingincreased the driver-yielding rate from 18 percent to 88 percent. 10 Pedestrian flashing beacons can use manual



School crossing



Pedestrian warning sign

Source: MUTCD 2009 edition

push buttons or automated passive (i.e., video or infrared) pedestrian detection, and should be unlit when not activated. Pedestrian flashing beacons typically receive power from standalone solar panels, but also may be wired to traditional power sources. It would cost between \$15,000 and \$20,000 to purchase and install two units (one on either side of a street). This includes solar panels, pad lighting, indication units, signage, all posts, and either passive infrared detection, or push buttons with audio instructions. MPO staff recommends a flashingbeacon strategy as part of the short- and long-term alternatives.

Medium-Term Improvements

Alternative 3: Reconfigure High Street Eastbound Approach Lanes and Tighten Curb Radius for Nahatan Street Right-Turn Lane

This alternative suggests reconfiguring lane assignment at the eastbound approach of High Street into one through lane and one right-turn-only lane, and tightening the curb line radius of Nahatan Street to allow right-turn movements to approach High Street more perpendicularly (Figure 6). The angle of the right-turn channelized lane should be no less than 70 degrees. This improvement would:

- Increase sight lines and distances, thus improving safety
- Reduce speeds of vehicles turning right on High Street
- Make traffic operations more efficient and allow right turns from Nahatan Street to enter High Street without merging at the entry point

Alternative 3 would not reduce traffic delay for Nahatan Street left-turn movement (Table 6 above).

¹⁰ Sherbutt, J., R. Van Houten, and S. Turner. "An Analysis of the Effects of Stutter Flash LED Beacons to Increase Yielding to Pedestrians Using Multilane Crosswalks." Presented at the Transportation Research Board Annual Meeting, Washington, DC, 2008.

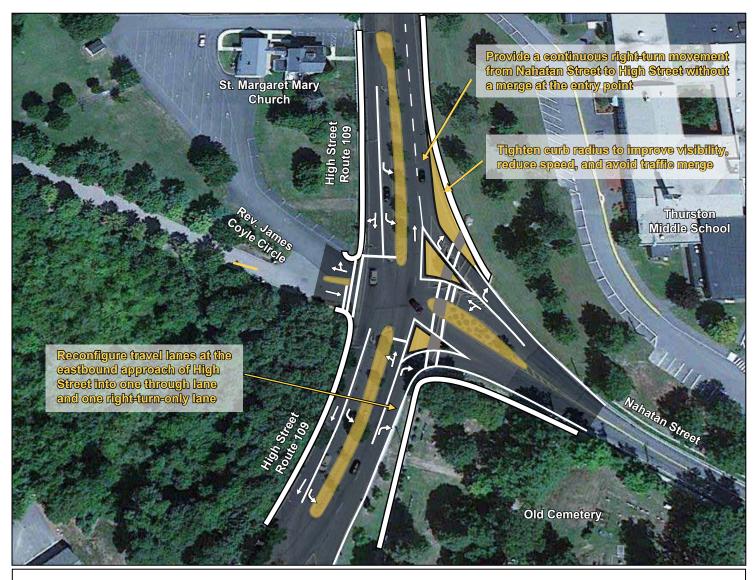


FIGURE 6 Medium-Term Improvement: Alternative 3 Reconfigure High Street Eastbound Approach Lanes

Safety and Operations Analyses at Selected Intersections—FFY 2014 This lane reconfiguration would reduce crashes by approximately 22 percent.¹¹ Further, providing full sight distance where it currently does not occur would reduce related crashes by approximately 20-to-37 percent.¹² It would cost between \$30,000 and \$50,000 to implement these modifications, including curbing, restriping, and signing.

Alternative 4: Tighten Curb Radius for Nahatan Street Right-Turn Lane
Alternative 4 is a variation of Alternative 3; it excludes reconfiguring High Street's eastbound approach lanes (Figure 7). Alternative 4 would tighten the Nahatan Street approach curb line radius in order to allow right-turn movement to approach High Street more perpendicularly, which would improve sight lines and distances and reduce speeds. In addition, it would add a stop-sign control for that movement. As in Alternative 3, the angle of the right-turn channelized lane should be no less than 70 degrees. This strategy is more costly than replacing a yield sign with a stop sign only (Alternative 1), but it is a more effective strategy for reducing crashes at a location with poor sight distance and a persistent crash pattern that cannot be improved with less expensive methods.

As in Alternative 3, providing full sight distance where it currently does not occur would reduce related crashes by approximately 20-to-37 percent. Table 6 (above) shows the results of the 2024 future year LOS analysis—Alternative 4 would not reduce traffic delays for Nahatan Street left-turn movement. It would cost between \$30,000 and \$50,000 to construct these improvements.

Long-Term Improvements

Alternative 5: Install New Traffic Signal

Installing a new traffic signal at the intersection would provide right-of-way assignment for traffic on Nahatan Street to enter High Street, reducing the large number of angle and rear-end crashes (Figure 8). Traffic signal warrant analysis shows that the intersection meets five of the nine warrants and justifies installing a traffic signal control (see Section 6). At present, the conduits, wiring, and interconnections for the traffic signal have been installed. In addition to the signalization, MPO staff recommends tightening the Nahatan Street approach curb-line radius in order to allow the right-turn movement to approach High Street more perpendicularly.

¹¹ Crash Modification Factors Clearinghouse, US Department of Transportation Federal Highway Administration, website, http://www.cmfclearinghouse.org/, December 17, 2014.

¹² Ibid.

¹³ Ibid



FIGURE 7
Medium-Term Improvement: Alternative 4
Tighten Curb Radius for Nahatan Street Right-Turn Lane

Safety and Operations Analyses at Selected Intersections—FFY 2014

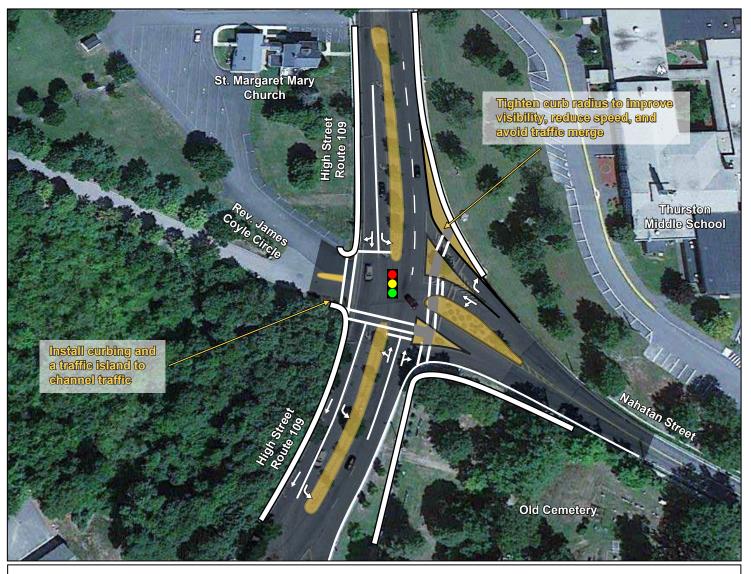


FIGURE 8
Long-Term Improvement
Alternative 5: Signalize Intersection

Safety and Operations Analyses at Selected Intersections—FFY 2014 Converting a two-way stop-sign control to a traffic-signal control could result in a 28-to-56 percent reduction in crashes. ¹⁴ Table 6 shows the results of the 2024 future year LOS analysis, which indicate that a traffic signal would improve overall traffic operations and reduce delays and queues at the intersection. Installing a traffic signal at the intersection would cost approximately \$1.5 million.

Alternative 6: Construct a Modern Roundabout

The design features of modern roundabouts encourage slower speeds, so are proven strategies for reducing severe-injury crashes. In addition, the yield-on-entry rule and one-way circulating flow of roundabouts reduce the number of conflict points and cut down on angle crashes significantly. Because of the safety and operational benefits of modern roundabouts, their appeal has risen throughout the Commonwealth in the past decade.¹⁵

Figure 9 shows the roundabout alternative and how it streamlines traffic circulation. The roundabout proposal includes the following features:

- A 120-foot inscribed circle diameter
- A 60-foot central-island diameter that incorporates a nine-foot mountable apron for use by trucks and emergency vehicles
- A 16- foot circulatory lane
- A two-lane entry for westbound High Street movements
- Slip lanes for Nahatan Street and High Street northbound right turns
- Additional crosswalks
- A rectangular rapid flashing beacon (RRFB) for the crosswalk across Nahatan Street

Converting a two-way stop control to a roundabout could reduce crashes by approximately 44-to-77 percent. Staff used Sidra intersection roundabout analysis software to analyze the roundabout alternative. Table 6 (above) shows the results of the 2024 future year analysis, which indicates that a roundabout would improve overall traffic operations and reduce delays and queues. Converting the intersection to a roundabout would cost approximately \$1.5-to-\$2.0 million.

¹⁴ Crash Modification Factors Clearinghouse, US Department of Transportation Federal Highway Administration, website, http://www.cmfclearinghouse.org/, December 17, 2014

¹⁵ In this document, the word roundabout refers to modern roundabouts that have a smaller central island and tighter deflection angle to slow down vehicles entering the roundabout and in the circulatory lane(s) to speeds between 20 and 25 mph.

¹⁶ Crash Modification Factors Clearinghouse, US Department of Transportation Federal Highway Administration.

¹⁷ Sidra Intersection 6, Akcelik and Associates Pty Limited, Greythorn, Victoria, Australia.

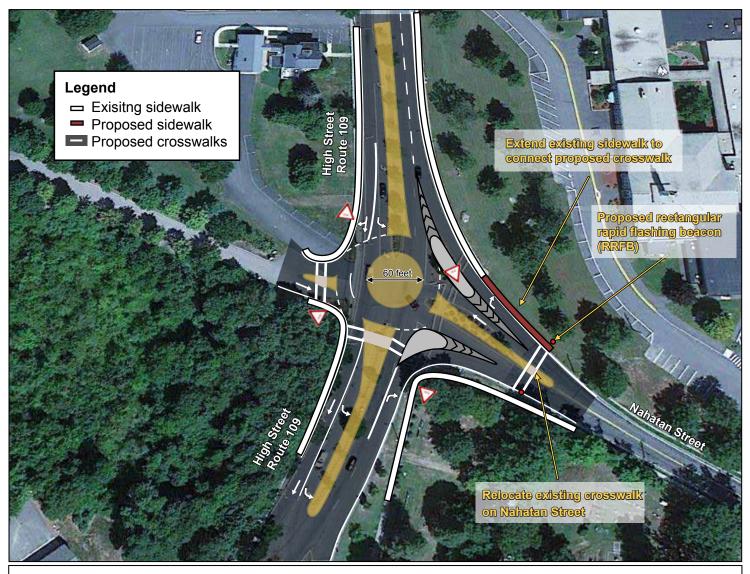


FIGURE 9
Long-Term Improvement
Alternative 6: Install a Roundabout

Safety and Operations Analyses at Selected Intersections—FFY 2014 In order for a roundabout to function well, it is important to prevent traffic queues from spreading into it, causing gridlock. The recurring traffic queue eastbound on High Street, which currently extends from the Hartford Avenue intersection into the Nahatan Street intersection, would prevent a roundabout from functioning well during peak periods.

8.2 High Street and Pond Street (near Sheehan School)

The concerns at the intersections are:

- Safety of pedestrians crossing at the intersection
- High speed of drivers turning right from High Street onto Pond Street drive because of a wide curb line radius
- All crashes at the intersection involve a driver attempting to enter High Street from Pond Street
- Traffic on Pond Street experiences long delays during peak periods

MPO staff developed and analyzed three short- and long-term alternatives for addressing safety and traffic operations at the intersection.

Short-Term Improvements

Alternative 1: Improve Sight Distance, Visibility, and Awareness of Intersection

Because vehicle-pedestrian conflicts are a significant problem in the channelized right-turn lane, it might be appropriate to provide signing to remind drivers of their legal obligation to yield to pedestrians crossing in the marked crosswalk. Advance street name (D3-2) signs identify an upcoming intersection and may be installed in advance of an unsignalized intersection. In addition, intersection warning signs for side roads, T-symbols (W2-2) and advance street name plaques (W16-8P) may be used where engineering judgment indicates a need to inform the road user in advance of an intersection.

Improved driver awareness and sight distance—as viewed from the Pond Street approach—such as flashing light-emitting diode (LED) stop signs and clearing some of the vegetation would reduce the number of right angle crashes. Increasing the triangle sight distance would reduce property-damage-only crashes by as much as 11 percent. ¹⁸

Pond Street Next Intersection

D3-2 Advance street name sign



Intersection warning sign

Pond Street

W16-8P Advance street name plaque

Source: MUTCD 2009 edition

¹⁸ Crash Modification Factors Clearinghouse, US Department of Transportation Federal Highway Administration.

LED stop sign

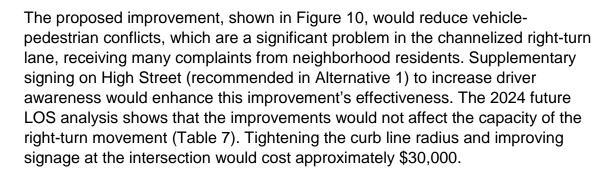
Source: safety.fhwa.dot.gov

Replacing standard stop signs with flashing LED stop signs would reduce angle-type crashes by as much as 41 percent. These improvements would cost approximately \$5,000.

Alternative 2: Tighten Curb Radius for High Street Eastbound Right Turns

This alternative would increase safety by:

- Forcing drivers turning right onto Pond Street to reduce their speeds
- Reducing crossing distance for pedestrians
- Improving sight distance at the intersection, especially for drivers turning right onto Pond Street, and Pond Street drivers turning left onto High Street
- Improving awareness of the intersection by bringing all turn movements to the intersection



Long-Term Improvements

Alternative 3: Install New Traffic Signal

Installing a new traffic signal—"walk-and-don't-walk" times for pedestrians and "green times" for traffic on High Street and Pond Street—would increase safety and reduce peak-period traffic delays. Traffic signal warrant analysis shows that the intersection meets three of the nine warrants and justifies installing a traffic signal control (see Section 6). Figure 11 shows the intersection layout for the proposed traffic signal, including tightening the curb line radius for High Street eastbound right-turn movements. Additional improvements include providing a crosswalk across High Street and pedestrian signals with pushbuttons and countdown timers.

Table 7 presents results of the 2024 future year LOS analysis, which indicate that installing a traffic signal would improve overall traffic operations. Converting a two-way stop control to a traffic signal would reduce total crashes by about 28-to-56 percent. ¹⁹ These improvements would cost approximately \$1.5 million.

¹⁹ Ihid.



FIGURE 10 Medium-Term Improvement: Alternative 2 Tighten Curb Radius for High Street Eastbound Right Turns

Safety and Operations Analyses at Selected Intersections—FFY 2014

TABLE 7
High Street and Pond Street Intersection (Near Sheehan School)
Future Year (2024) Peak-Hour Level of Service

	Move	AM	AM	AM	PM	PM	PM
Intersection/Approach	ment	LOS	Delay ^a	Queue ^b	LOS	Delay	LOS
2014 Existing Conditions							
High St Eastbound	T+R	Α	0	0	Α	0	0
High St Westbound	L+T	Α	0	0	Α	0	0
Pond St Northbound	L	F	114.5	225	F	152.9	350
Pond St Northbound	T+R	В	14.4	25	Α	9.8	5
Total Intersection	All	С	17.8		D	28.6	
2024 Alternative 2:							
Reduce Curb Line							
High St Eastbound	T+R	Α	0	0	Α	0	0
High St Westbound	L+T	Α	0.1	0	Α	8.5	25
Pond St Northbound	L	F	149.7	275	F	>180	425
Pond St Northbound	T+R	В	14.8	10	Α	9.9	25
Total Intersection	All	С	23.5		D	34.8	
2024 Alternative 3: Install							
Traffic Signal							
High St Eastbound	Т	В	18	#590	В	14.2	305
High St Eastbound	R	Α	6.1	145	Α	4.6	63
High St Westbound	L	В	11.2	26	Α	12.1	42
High St Westbound	Т	Α	9.8	198	С	26.1	#750
Pond St Northbound	L	D	42.6	#290	D	48.5	#365
Pond St Northbound	R	Α	0.1	13	Α	8.8	31
Total Intersection	All	В	16.2		С	23.6	

^a Delay in seconds per vehicle. ^b 95th percentile queue length in feet. # = The 95th percentile volume exceeds capacity.

Source: Central Transportation Planning Staff.



FIGURE 11
Long-Term Improvement
Alternative 3: Install Traffic Signal

Safety and Operations Analyses at Selected Intersections–FFY 2014

9 RECOMMENDATIONS AND DISCUSSIONS

The above evaluations indicate that the intersections of High at Nahatan Streets and Pond Street need improvements to increase safety and reduce congestion. MPO staff has developed six alternatives to improve safety and traffic operations at the Nahatan Street intersection, and three alternatives to improve safety at the Pond Street intersection. Cost and effectiveness are primary factors in selecting the preferred alternatives.

9.1 High Street and Nahatan Street Intersection

- Alternative 1 is a short-term, low-cost improvement—it does not fully address the safety and traffic operations problems at the intersection.
- Alternative 2 is a short-term, low-cost improvement that addresses safety for pedestrians crossing High Street at Saint Margaret Mary Church. We also recommended it as a medium- and long-term alternative. This alternative does not address safety and operations at the intersection.
- Alternatives 3 and 4 are medium-term, low-cost improvements—they
 address the safety and operations problems at the intersection and are
 more cost effective than the short-term improvements. Alternative 3 is
 preferable to Alternative 4 because it has more safety benefits and
 simplifies traffic movements through the intersection.
- Alternatives 5 and 6 are long-term, high-cost improvements—they
 address the safety and operations problems. Alternative 5 is preferable
 to Alternative 6 because the improvements are within the right-of-way and
 do not alter intersection layout as much as Alternative 6. In addition,
 Alternative 6 would not function well unless an eastbound traffic queue
 downstream of the intersection was addressed.

MPO staff recommends Alternative 3 for short- and medium-term improvements. These modifications would improve safety by increasing sight lines and distances; reduce speeds of vehicles turning right onto High Street, and make traffic operations more efficient by reducing merging maneuvers.

For long-term improvements, MPO staff recommend Alternative 5, which would provide all of the safety benefits of Alternative 3. In addition, Alternative 5 would provide orderly movement of traffic (vehicular and pedestrian) and reduce the frequency and severity of crashes. Alternative 5 also would reduce traffic congestion, but Alternative 3 would not. The conduits, wiring, and interconnections required for installing a traffic signal already have been installed, which would facilitate implementation.

9.2 High Street and Pond Street Intersection (near Sheehan School):

- **Alternative 1** is a short-term, low-cost improvement; however, it does not fully address pedestrian safety problems.
- Alternative 2 is a medium-term, low-cost improvement, and it does address pedestrian safety and traffic operations problems. Alternative 2 is the most cost-effective improvement and is recommended by MPO staff.
- Alternative 3 is a long-term, high-cost improvement, and it addresses safety and operations problems. Alternative 3 should be considered if the improvements in Alternative 2 do not address the pedestrian safety problem.

9.3 Next Steps

This study gives the Town of Westwood an opportunity look at the needs of these intersections and plan for design and engineering. Following this planning study, the next steps are to implement the preferred low-cost, short-term improvements. Implementation of the long-term, high-cost improvements hinge upon cooperation between MassDOT, Westwood, and the MPO to begin the project notification and review process, complete a project initiation form, and initiate the preliminary design and engineering necessary to place the project on the Transportation Improvement Program (TIP). Appendix E contains MassDOT project development process for highway projects. Finally, the study supports the MPO's visions and goals, which include increasing transportation safety, preserving and maintaining the transportation system, and advancing mobility, access and congestion reduction.

SA/sa

Cc: Michael Jaillet, Town Administrator, Westwood

APPENDIX A

Public Participation

- 1. Letter from Town of Westwood
- 2. Advisory Task Force
- 3. Comments from Advisory Task Force and MassDOT Highway Division District 6



TOWN OF WESTWOOD

COMMONWEALTH OF MASSACHUSETTS BOARD OF SELECTMEN

Nancy C. Hyde, Chairman Philip N. Shapiro, Clerk Patrick J. Ahearn, Third Member

Michael A. Jaillet, Town Administrator Pamela M. Dukeman, Finance Director Christine E. McCarthy, Executive Assistant

November 12, 2013

Karl Quackenbush, Executive Director Central Transportation Planning Staff 10 Park Plaza, Suite 2150 Boston, MA 02116-3968

Dear Karl:



The Board of Selectmen, the Planning Board, the DPW, the Police Department, and the Pedestrian/Bicycle Safety Committee of the Town of Westwood have recently reviewed the list of problem intersections in Westwood. The following intersections have all been suggested by Town representatives in the past as being in need of study to address existing safety and congestion problems. The Town desires to make this list available to CTPS so that these problem intersections may be considered by MPO staff when selecting intersections or corridor segments for study under various UPWP studies, such as *Safety and Operations Analyses at Selected Intersections – FFY 2014*.

The purpose of this letter is to reaffirm that these intersections are in need of study, and to express the Town's intention to cooperate with and support the MPO in any MPO planning effort. The Town will strive to implement improvements recommended by any such studies, given the appropriateness of the improvements and the Town's ability to fund them.

The intersections are as follows:

- High Street (Route 109) and Nahatan Street safety/congestion
- High Street (Route 109) and Pond Street safety
- Washington Street (Route 1A) and Everett Street/Clapboardtree Street safety and congestion
- Washington Street (Route 1A), East Street and School Street safety and congestion
- High Street (Route 109) and Summer Street congestion
- Winter Street and Clapboardtree Street safety

The intersection of Nahatan Street and Clapboardtree Street has been previously listed as a problem intersection, but planning for improvements to this intersection is being pursued by local means at this time, and so it no longer needs to be considered for MPO study.

Sincerely,

Michael Jaillet

Town Administrator

Study Advisory Task Force

Michael Jaillet, Town Administrator

Todd Korchin, DPW Director

Jeffrey Bina, Town Engineer

Paul Sicard, Westwood Police Department

Steve Olanoff, Westwood Pedestrian and Bicycle Committee



TOWN OF WESTWOOD COMMONWEALTH OF MASSACHUSETTS

DEPARTMENT OF PUBLIC WORKS

TODD KORCHIN, DPW DIRECTOR BRENDAN RYAN, STREETS & GROUNDS SUPERINTENDENT JEFFREY BINA, P.E., TOWN ENGINEER

October 10, 2014

Seth A. Asante, P.E.
Principal Transportation Planner
Central Transportation Planning Staff
10 Park Plaza, Suite 2150
Boston, MA 02116

Re:

Review Comments, Safety and Operations Analysis in Westwood, MA at, High Street (Route 109) at Nahatan Street and,

High Street (Route 109) at Pond Street

Dear Mr. Asante,

Thank you for coming on September 29, 2014 to present your findings on the analysis of the above referenced intersections. We have summarized the items we discussed in order to further the development of proposed improvements at those intersections.

High Street at Nahatan Street

Of the options presented the group agreed to the dedicated lanes on High St. NB for the right turn onto Nahatan Street and the dedicated lane for vehicles coming onto High St. NB from Nahatan St. This configuration was shown on Fig. 4 of the analysis. The group also recommended a new curbing layout that would be installed in the locations that show the white pavement marking gore lines on that same Fig. 4. One modification to that layout was the addition of the stop sign and curbing relocation recommended in Fig. 5 for the vehicles approaching High St. NB from Nahatan St.

High Street at Pond Street

Both the short and medium term strategy presented emphasize increasing the visibility of the movement at the intersection. This would obviously help with the driver approaching the intersection however, the group was concerned that neither of them addressed the main concern of pedestrian safety. The consensus was that vehicles traveling High St. NB turning onto Pond St. would enter the turn at a high rate of speed thereby making the pedestrian crossing undesireable. A better alternative suggested was to decrease the radius of the curve along the curb at the High St. NB/Nahatan St. right turn. This would serve two purposes: 1—shorten the distance pedestrians would have to travel and 2 – cause vehicles to decrease their speed to negotiate the sharper turn onto Pond St.

Very truly yours,

Jeffrey J. Bina, PE

Town Engineer

cc:

Michael Jaillet, Town Administrator

Todd Korchin, DPW director

Paul Sicard, Westwood Police Department

Steve Olanoff, Westwood Pedestrian and Bicycle Committee

Seth Asante

From:

Lipton, Amitai (DOT)

Sent:

Thursday, December 11, 2014 2:29 PM

To:

'Seth Asante'

Cc:

Kulen, Raj (DOT)

Subject:

RE: Safety and Operations Analyses at Selected Intersections: Westwood Intersections

Hi Seth,

The District 6 Traffic section has reviewed the CTPS memorandum dated 11/20/2014 regarding two intersections in the Town of Westwood, and offers the following comments:

- 1. Table 4 LOS F at stop-controlled approaches is very common, and does not necessarily constitute an unacceptable situation. The queues on Nahatan St do not exceed 6 vehicles (150 ft), indicating that there may not be severe congestion. However, the longer queues on Pond St (14 vehicles) and excessive control delay (2 minutes or more) could be considered unacceptable.
- 2. Section 7.1 Other short- and long-term alternatives should be considered. From aerial photography, it appears that inconsistent and/or confusing signage and pavement markings in the existing condition may be a contributing factor to the safety problem. A short-term measure could include replacing signs and markings with a clearer design.

It is not clear, given the geometry, that drivers would take heed of a STOP sign (Alt. 1). A PHB or RRFB may be appropriate at the existing CW in front of the church (Alt. 2), but the proximity of driveways should be taken into account. It is not clear what the benefit of adding STOP control to High St would be (Alt. 3). Alternatives 4, 5, and particularly 6 appear to have merit, although Alt. 4 might be modified to tighten up the entire intersection. For all alternatives, the intersection design should consider a 4-legged intersection, with the driveway as the fourth leg. Visibility screening, while typically used for approaches to circular intersections, may be an effective tool in lowering speeds on the Nahatan St RT approach, and may also reduce the incidence of rear-end collisions.

- 3. Figure 6 We do not agree with the concept plan of installing STOP control at an added-lane condition. We also do not agree with placing a crosswalk before a stop line. If the desire is to improve pedestrian safety, the angle of a right-turn channelized lane should be no less than 70 degrees.
- 4. Figure 9 This concept plan appears to provide a good solution to the safety and operational concerns at this location. It also has the added benefit of providing an opportunity for adjacent Pond St traffic to effectively turn left onto High St, a movement that is not allowed at the existing intersection. Certain modified design features should be considered: (a) SB approach having L+TR lanes, with only 1 departing lane to the south; (b) spiral lane design; (c) 70 degree channelized turn lane for NB approach; and (d) Danish-style crossing on southerly and possibly easterly leg of the roundabout.
- 5. Section 7.2 The R10-15 signs are intended solely for use at signalized intersection, and should not be used at unsignalized locations, nor in advance of an intersection. An interim option for enhanced visibility STOP signs would be to install red reflective stripe on the sign post. As a short-term measure, additional advance signage on High St (D3-2, W2-2, W2-3, W16-8P, etc.) would notify drivers of an approaching intersection. An additional alternative scenario should consider whether a roundabout would be appropriate at this location.
- 6. Figure 11 A crosswalk should also be provided across High St.

If you have any questions, or would like further information about these comments, please do not hesitate to contact me.

Amitai Lipton
District 6 Traffic Engineer
MassDOT Highway Division
185 Kneeland St
Boston MA 02111
amitai.lipton@state.ma.us
857.368.6313 (office)
617.892.3171 (mobile)

APPENDIX B

Turning-Movement Count Data

File Name: Nahatan AM+MID+PM

Site Code : 04081422 Start Date : 4/8/2014

																Pa	ge No	: 1			
										utos - He	avy Vehic										1
			High St					ahatan S					High St					v Coyle (
Ot and Time	Dialet		rom Nort			District		rom Eas			Dimbd		om Sout			District		om Wes			1-4 T-4-1
Start Time 07:00 AM	Right	Thru	Left	Peds /	App. Total 162	Right	Thru	Left 16	Peds A		Right	Thru 184	Left 0	<u>Peas</u> A	App. Total 265	Right 0	Thru 0	Left	Peas	App. Total	Int. Total 469
07.00 AM 07:15 AM	5 0	93 83	64 77	0	162	25 62	0 0	30	1	41 93	81 81	177	0	0	258	1	0	0 0	0	1	512
07:13 AM 07:30 AM	1	111	67	0	179	54	0	27	1	82	91	181	1	0	273	0	0	0	11	11	545
07:45 AM	0	87	37	0	124	46	2	22	Ö	70	60	165	Ö	0	225	0	0	0	0	0	419
Total	6	374	245	0	625	187	2	95	2	286	313	707	1	0	1021	1	0	0	12	13	1945
į										,											'
08:00 AM	0	91	21	0	112	42	0	8	0	50	39	193	0	0	232	1	0	0	0	1	395
08:15 AM	0	119	43	0	162	41	0	16	0	57	34	187	3	0	224	0	0	0	0	0	443
08:30 AM	2	99	32	0	133	29	0	14	0	43	55	205	1	0	261	1	0	0	2	3	440
08:45 AM Total	<u>4</u> 6	84 393	37 133	0	125 532	37 149	2	18 56	0	57 207	33 161	225 810	<u>0</u> 4	0	258 975	3	0	0	<u>4</u> 6	<u>5</u> 9	445 1723
Total	0	393	133	U	532	149	2	50	U	207	101	010	4	U	9/5	3	U	U	0	9	1723
*** BREAK ***																					
11:00 AM	1	98	36	0	135	24	1	22	0	47	16	109	1	3	129	1	0	0	2	3	314
11:15 AM	0	115	23	0	138	26	2	11	0	39	24	135	1	2	162	0	1	0	0	1	340
11:30 AM	3	134	45	1	183	50	0	14	0	64	29	138	1	0	168	1	1	0	0	2	417
11:45 AM	1	126	73	0	200	35	0	18	0	53	64	127	2	1	194	0	1	0	1	2	449
Total	5	473	177	1	656	135	3	65	0	203	133	509	5	6	653	2	3	0	3	8	1520
12:00 PM	0	131	58	0	189	65	0	48	3	116	22	137	0	0	159	0	0	0	2	2	466
12:15 PM	1	138	38	Ő	177	53	0	22	0	75	18	139	0	0	157	0	0	1	0	1	410
12:30 PM	1	121	41	Ö	163	42	Ö	12	5	59	25	137	ő	2	164	Ö	Ö	Ö	2	2	388
12:45 PM	1	151	47	0	199	30	0	13	0	43	24	139	0	0	163	0	0	0	0	0	405
Total	3	541	184	0	728	190	0	95	8	293	89	552	0	2	643	0	0	1	4	5	1669
01:00 PM	1	111	32	1	145	70	1	25	0	96	17	109	0	0	126	0	0	0	1	1	368
01:15 PM	0	114	35	0	149	27	Ó	10	4	41	16	113	0	0	129	0	0	1	Ó	1	320
01:30 PM	3	133	32	Ö	168	42	Ö	19	0	61	12	152	1	0	165	1	0	0	4	5	399
01:45 PM	2	155	31	Ö	188	37	Ö	16	Ö	53	10	124	0	Ö	134	0	Ö	1	1	2	377
Total	6	513	130	1	650	176	1	70	4	251	55	498	1	0	554	1	0	2	6	9	1464
*** BREAK ***																					
03:00 PM	0	202	47	0	249	41	1	16	0	58	15	122	1	2	140	0	0	1	5	6	453
03:00 PM 03:15 PM	0	202	58	0	260	50	0	22	6	78	31	144	0	5	180	1	0	0	1	2	520
03:30 PM	0	174	60	0	234	38	0	29	1	68	33	134	1	3	171	Ó	0	0	1	1	474
03:45 PM	1	195	57	0	253	43	1	14	Ö	58	31	134	7	0	172	1	0	0	i	2	485
Total	1	773	222	0	996	172	2	81	7	262	110	534	9	10	663	2	0	1	8	11	1932
04:00 PM	0	188	35	0	223	35	1	24	3	63	29	131	4	0	164	5	1	0	8	14	464
04:15 PM	0	200	46	0	246	46	Ö	24	1	71	9	128	1	0	138	1	Ö	0	0	1	456
04:30 PM	Ő	211	56	Ő	267	42	Ö	26	0	68	22	122	0	Ö	144	0	1	Ő	2	3	482
					- 1					1											

File Name: Nahatan AM+MID+PM

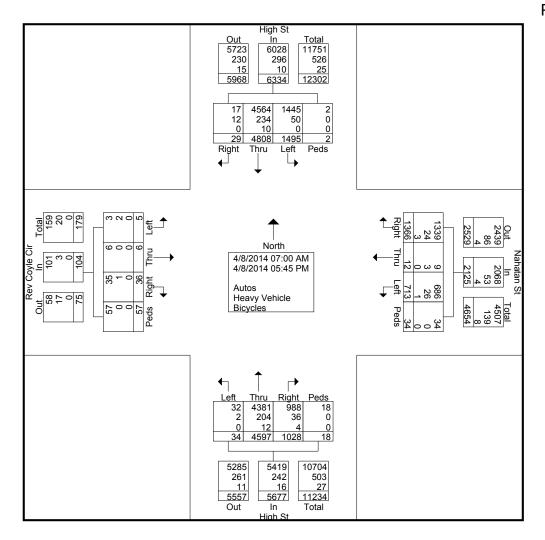
Site Code : 04081422 Start Date : 4/8/2014

Page No : 2

Groups Printed- Autos - Heavy Vehicle - Bicycles

										Autos - ne	avy verill	ic - Dicy							_		
			High St				N	ahatan S	St				High St				Re	v Coyle	Cir		
		F	rom Nort	th			F	rom Eas	st			F	rom Sou	th			Fi	rom Wes	st		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
04:45 PM	2	231	56	0	289	54	0	36	3	93	24	114	7	0	145	3	0	0	1	4	531
Total	2	830	193	0	1025	177	1	110	7	295	84	495	12	0	591	9	2	0	11	22	1933
05:00 PM	0	224	54	0	278	49	1	31	0	81	22	126	2	0	150	18	1	1	0	20	529
05:15 PM	0	216	48	0	264	46	0	34	3	83	20	135	0	0	155	0	0	0	0	0	502
05:30 PM	0	233	49	0	282	56	0	47	1	104	23	122	0	0	145	0	0	0	6	6	537
05:45 PM	0	238	60	0	298	29	0	29	2	60	18	109	0	0	127	0	0	0	1	1	486
Total	0	911	211	0	1122	180	1	141	6	328	83	492	2	0	577	18	1	1	7	27	2054
Grand Total	29	4808	1495	2	6334	1366	12	713	34	2125	1028	4597	34	18	5677	36	6	5	57	104	14240
Apprch %	0.5	75.9	23.6	0		64.3	0.6	33.6	1.6		18.1	81	0.6	0.3		34.6	5.8	4.8	54.8		
Total %	0.2	33.8	10.5	0	44.5	9.6	0.1	5	0.2	14.9	7.2	32.3	0.2	0.1	39.9	0.3	0	0	0.4	0.7	
Autos	17	4564	1445	2	6028	1339	9	686	34	2068	988	4381	32	18	5419	35	6	3	57	101	13616
% Autos	58.6	94.9	96.7	100	95.2	98	75	96.2	100	97.3	96.1	95.3	94.1	100	95.5	97.2	100	60	100	97.1	95.6
Heavy Vehicle	12	234	50	0	296	24	3	26	0	53	36	204	2	0	242	1	0	2	0	3	594
% Heavy Vehicle	41.4	4.9	3.3	0	4.7	1.8	25	3.6	0	2.5	3.5	4.4	5.9	0	4.3	2.8	0	40	0	2.9	4.2
Bicycles	0	10	0	0	10	3	0	1	0	4	4	12	0	0	16	0	0	0	0	0	30
% Bicycles	0	0.2	0	0	0.2	0.2	0	0.1	0	0.2	0.4	0.3	0	0	0.3	0	0	0	0	0	0.2

Site Code : 04081422 Start Date : 4/8/2014

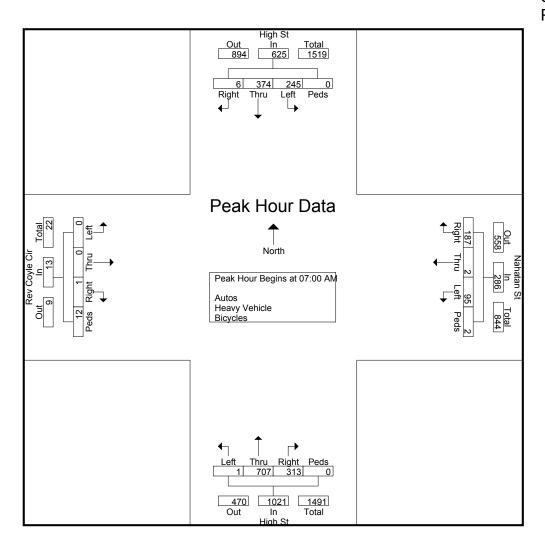


File Name: Nahatan AM+MID+PM

Site Code : 04081422 Start Date : 4/8/2014

			High St				N	lahatan :	St				High St				Re	v Coyle	Cir		
		F	rom Nor	th			F	rom Eas	st			Fi	rom Sou	th			F	rom We	st		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysi	is From 07	7:00 AM t	o 09:45 /	AM - Pea	ak 1 of 1																
Peak Hour for Enti	ire Interse	ction Beg	ins at 07	:00 AM																	
07:00 AM	5	93	64	0	162	25	0	16	0	41	81	184	0	0	265	0	0	0	1	1	469
07:15 AM	0	83	77	0	160	62	0	30	1	93	81	177	0	0	258	1	0	0	0	1	512
07:30 AM	1	111	67	0	179	54	0	27	1	82	91	181	1	0	273	0	0	0	11	11	545
07:45 AM	0	87	37	0	124	46	2	22	0	70	60	165	0	0	225	0	0	0	0	0	419
Total Volume	6	374	245	0	625	187	2	95	2	286	313	707	1	0	1021	1	0	0	12	13	1945
% App. Total	1	59.8	39.2	0		65.4	0.7	33.2	0.7		30.7	69.2	0.1	0		7.7	0	0	92.3		
PHF	.300	.842	.795	.000	.873	.754	.250	.792	.500	.769	.860	.961	.250	.000	.935	.250	.000	.000	.273	.295	.892

Site Code : 04081422 Start Date : 4/8/2014

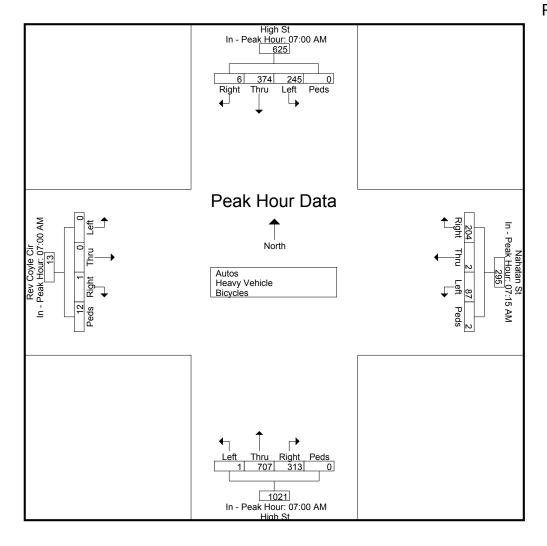


File Name: Nahatan AM+MID+PM

Site Code : 04081422 Start Date : 4/8/2014

			High St				N	lahatan :	St				High St				Re	v Coyle	Cir		
		F	rom Nor	th			F	rom Eas	st			F	rom Sou	th			F	rom Wes	st		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int.
Peak Hour Analys	sis From 0	7:00 AM 1	o 09:45	AM - Pea	ak 1 of 1	-										-					
Peak Hour for Ea	ch Approa	ch Begins	at:																		_
	07:00 AM	1				07:15 AM					07:00 AM					07:00 AM					
+0 mins.	5	93	64	0	162	62	0	30	1	93	81	184	0	0	265	0	0	0	1	1	
+15 mins.	0	83	77	0	160	54	0	27	1	82	81	177	0	0	258	1	0	0	0	1	
+30 mins.	1	111	67	0	179	46	2	22	0	70	91	181	1	0	273	0	0	0	11	11	
+45 mins.	0	87	37	0	124	42	0	8	0	50	60	165	0	0	225	0	0	0	0	0	
Total Volume	6	374	245	0	625	204	2	87	2	295	313	707	1	0	1021	1	0	0	12	13	
% App. Total	1	59.8	39.2	0		69.2	0.7	29.5	0.7		30.7	69.2	0.1	0		7.7	0	0	92.3		
DHE	300	2/2	705	000	973	833	250	725	500	703	860	061	250	000	035	250	000	000	272	205	1

Site Code : 04081422 Start Date : 4/8/2014

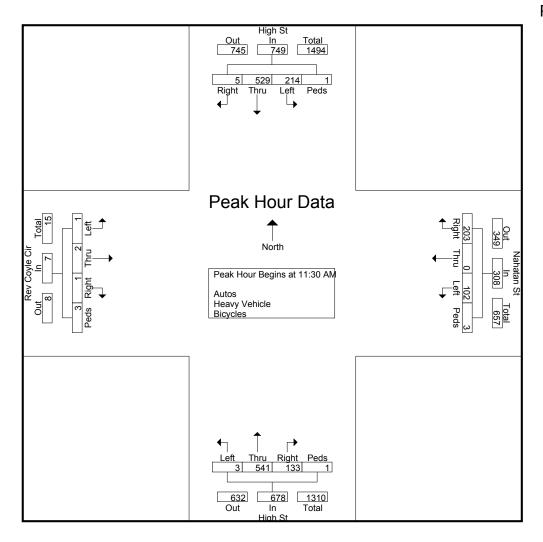


File Name: Nahatan AM+MID+PM

Site Code : 04081422 Start Date : 4/8/2014

			High St				N	lahatan :	St				High St				Re	v Coyle	Cir		ĺ
		F	rom Nort	th			F	rom Eas	st			F	rom Sou	th			F	rom We	st		<u> </u>
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysi	is From 10	0:00 AM t	o 01:45 F	PM - Pea	ak 1 of 1																
Peak Hour for Enti	ire Interse	ction Beg	ins at 11	:30 AM																	
11:30 AM	3	134	45	1	183	50	0	14	0	64	29	138	1	0	168	1	1	0	0	2	417
11:45 AM	1	126	73	0	200	35	0	18	0	53	64	127	2	1	194	0	1	0	1	2	449
12:00 PM	0	131	58	0	189	65	0	48	3	116	22	137	0	0	159	0	0	0	2	2	466
12:15 PM	1	138	38	0	177	53	0	22	0	75	18	139	0	0	157	0	0	1	0	1	410
Total Volume	5	529	214	1	749	203	0	102	3	308	133	541	3	1	678	1	2	1	3	7	1742
% App. Total	0.7	70.6	28.6	0.1		65.9	0	33.1	1		19.6	79.8	0.4	0.1		14.3	28.6	14.3	42.9		
PHF	.417	.958	.733	.250	.936	.781	.000	.531	.250	.664	.520	.973	.375	.250	.874	.250	.500	.250	.375	.875	.935

Site Code : 04081422 Start Date : 4/8/2014

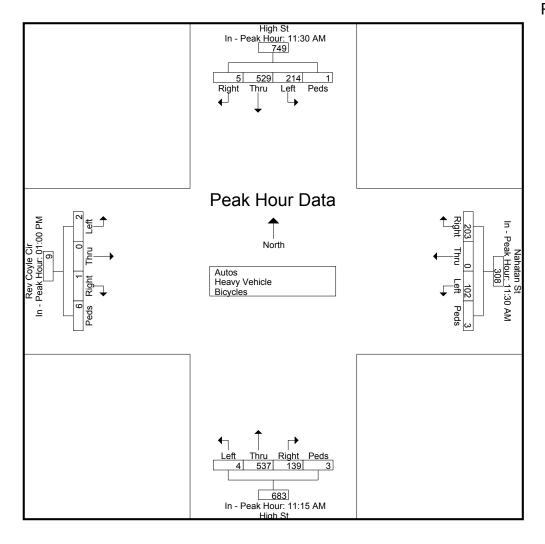


File Name: Nahatan AM+MID+PM

Site Code : 04081422 Start Date : 4/8/2014

			High St				N	Nahatan S	St				High St				Re	v Coyle	Cir		
		F	rom Nor	th			F	From Eas	st			F	rom Sou	th			F	rom Wes	st		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. To
Peak Hour Analys	sis From 10	0:00 AM t	o 01:45 I	PM - Pe	ak 1 of 1	-					_										
Peak Hour for Ea	ch Approac	h Begins	at:																		_
	11:30 AM	_				11:30 AM					11:15 AM					01:00 PM					
+0 mins.	3	134	45	1	183	50	0	14	0	64	24	135	1	2	162	0	0	0	1	1	
+15 mins.	1	126	73	0	200	35	0	18	0	53	29	138	1	0	168	0	0	1	0	1	
+30 mins.	0	131	58	0	189	65	0	48	3	116	64	127	2	1	194	1	0	0	4	5	
+45 mins.	1	138	38	0	177	53	0	22	0	75	22	137	0	0	159	0	0	1	1	2	
Total Volume	5	529	214	1	749	203	0	102	3	308	139	537	4	3	683	1	0	2	6	9	
% App. Total	0.7	70.6	28.6	0.1		65.9	0	33.1	1		20.4	78.6	0.6	0.4		11.1	0	22.2	66.7		
PHF	417	958	733	250	936	781	000	531	250	664	543	973	500	375	880	250	000	500	375	450	

Site Code : 04081422 Start Date : 4/8/2014

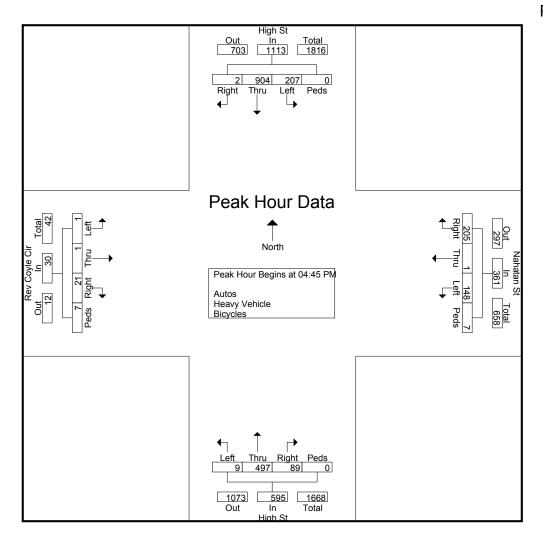


File Name: Nahatan AM+MID+PM

Site Code : 04081422 Start Date : 4/8/2014

			High St				N	lahatan :	St				High St				Re	v Coyle	Cir		•
		F	rom Nort	th			F	rom Eas	st			F	rom Sou	th			F	rom Wes	st		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysi	is From 02	2:00 PM t	o 05:45 F	PM - Pea	ak 1 of 1																
Peak Hour for Enti	ire Interse	ction Beg	ins at 04	:45 PM																	
04:45 PM	2	231	56	0	289	54	0	36	3	93	24	114	7	0	145	3	0	0	1	4	531
05:00 PM	0	224	54	0	278	49	1	31	0	81	22	126	2	0	150	18	1	1	0	20	529
05:15 PM	0	216	48	0	264	46	0	34	3	83	20	135	0	0	155	0	0	0	0	0	502
05:30 PM	0	233	49	0	282	56	0	47	1	104	23	122	0	0	145	0	0	0	6	6	537
Total Volume	2	904	207	0	1113	205	1	148	7	361	89	497	9	0	595	21	1	1	7	30	2099
% App. Total	0.2	81.2	18.6	0		56.8	0.3	41	1.9		15	83.5	1.5	0		70	3.3	3.3	23.3		
PHF	.250	.970	.924	.000	.963	.915	.250	.787	.583	.868	.927	.920	.321	.000	.960	.292	.250	.250	.292	.375	.977

Site Code : 04081422 Start Date : 4/8/2014

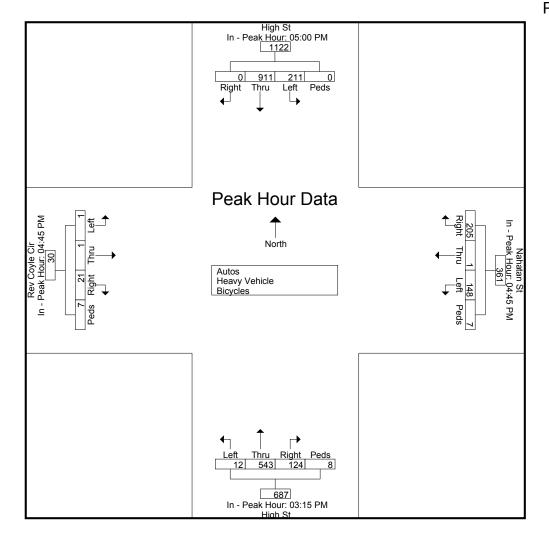


File Name: Nahatan AM+MID+PM

Site Code : 04081422 Start Date : 4/8/2014

			High St				N	ahatan S	St				High St				Re	v Coyle	Cir		
		F	rom Nort	h			F	rom Eas	t			Fi	rom Sout	h			F	rom Wes	st		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analys	is From 0	2:00 PM t	o 05:45 F	PM - Peak	(1 of 1	_					_										
Peak Hour for Eac	ch Approa	ch Begins	at:																		_
	05:00 PM	1				04:45 PM					03:15 PM					04:45 PM					
+0 mins.	0	224	54	0	278	54	0	36	3	93	31	144	0	5	180	3	0	0	1	4	
+15 mins.	0	216	48	0	264	49	1	31	0	81	33	134	1	3	171	18	1	1	0	20	
+30 mins.	0	233	49	0	282	46	0	34	3	83	31	134	7	0	172	0	0	0	0	0	
+45 mins.	0	238	60	0	298	56	0	47	1	104	29	131	4	0	164	0	0	0	6	6	
Total Volume	0	911	211	0	1122	205	1	148	7	361	124	543	12	8	687	21	1	1	7	30	
% App. Total	0	81.2	18.8	0		56.8	0.3	41	1.9		18	79	1.7	1.2		70	3.3	3.3	23.3		
PHF	.000	.957	.879	.000	.941	.915	.250	.787	.583	.868	.939	.943	.429	.400	.954	.292	.250	.250	.292	.375	

Site Code : 04081422 Start Date : 4/8/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (near Nahatan St) 04/08/14 PM and 04/17/14 AM

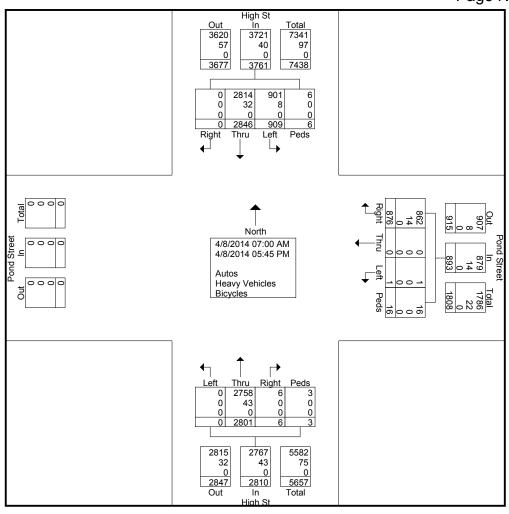
File Name: Pond near Nahatan AM and PM

Site Code : 04081423 Start Date : 4/8/2014

						Groups Prin	ted- Autos	- Heavy Vel	nicles - Bio	cycles	,	,				
			High S			•		Pond Street					High St			
			From No					From East					From South			
Start Time					App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
07:00 AM		-			89	57	0	0	1	58	0	219	0	0	219	366
07:15 AM		8			101	70	0	0	0	70	0	176	0	0	176	347
07:30 AM		8			122	71	0	0	0	71	0	188	0	0	188	381
07:45 AM					109	45	0	0	0	45	0	164	0	0	164	318
Tota	ıl 0	33	0 9	1 0	421	243	0	0	1	244	0	747	0	0	747	1412
08:00 AM					100	63	0	0	0	63	0	169	0	0	169	332
08:15 AM		-			137	46	0	0	1	47	0	172	0	0	172	356
08:30 AM		8			108	72	0	0	0	72	3	182	0	0	185	365
08:45 AM		8			106	45	0	0	0	45	0	218	0	0	218	369
Tota	ıl 0	34	3 10	3 0	451	226	0	0	1	227	3	741	0	0	744	1422
*** BREAK ***																
03:00 PM	л	15			215	25	0	0	3	28	1	94	0	2	97	340
03:15 PM	л O	17	1 50) 4	225	31	0	0	0	31	0	119	0	0	119	375
03:30 PM	л	14	9 4	1 0	193	31	0	0	1	32	0	126	0	0	126	351
03:45 PM	л <u> </u>	15	3 5	3 0	206	43	0	0	0	43	1	122	0	1	124	373
Tota	ıl 0	62	7 20	3 4	839	130	0	0	4	134	2	461	0	3	466	1439
04:00 PM					223	36	0	0	2	38	0	126	0	0	126	387
04:15 PM					225	36	0	0	3	39	0	84	0	0	84	348
04:30 PM		17	2 54	1 0	226	37	0	0	2	39	1	111	0	0	112	377
04:45 PM	<i>I</i> 0	22			282	46	0	0	0	46	0	105	0	0	105	433
Tota	ıl 0	74	5 21	1 0	956	155	0	0	7	162	1	426	0	0	427	1545
05:00 PM					286	35	0	1	1	37	0	117	0	0	117	440
05:15 PM					249	34	0	0	1	35	0	114	0	0	114	398
05:30 PM					292	28	0	0	0	28	0	108	0	0	108	428
05:45 PM					267	25	0	0	1	26	0	87	0	0	87	380
Tota	ıl 0	80	1 29	1 2	1094	122	0	1	3	126	0	426	0	0	426	1646
Grand Tota					3761	876	0	1	16	893	6	2801	0	3	2810	7464
Apprch %	6 0					98.1	0	0.1	1.8		0.2	99.7	0	0.1		
Total %	6 0				50.4	11.7	0	0	0.2	12	0.1	37.5	0	0	37.6	
Autos					3721	862	0	1	16	879	6	2758	0	3	2767	7367
% Autos					98.9	98.4	0	100	100	98.4	100	98.5	0	100	98.5	98.7
Heavy Vehicles		-		0	40	14	0	0	0	14	0	43	0	0	43	97
— % Heavy Vehicles						1.6	0	0	0	1.6	0	1.5	0	0	1.5	1.3
Bicycles				0	0	0	0	0	0	0	0	0	0	0	0	0
% Bicycles	s 0		0 () 0	0	0	0	0	0	0	0	0	0	0	0	0

File Name: Pond near Nahatan AM and PM

Site Code : 04081423 Start Date : 4/8/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (near Nahatan St) 04/08/14 PM and 04/17/14 AM

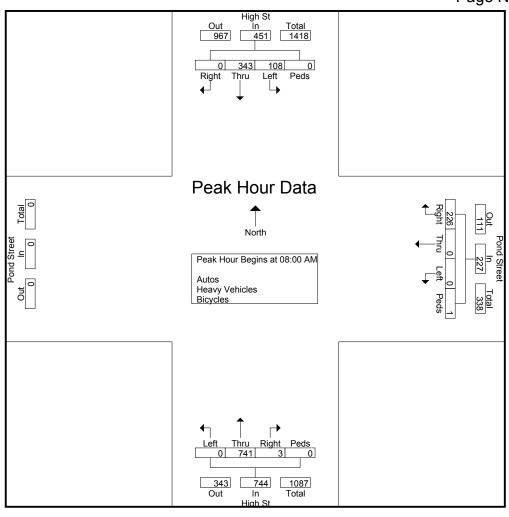
File Name: Pond near Nahatan AM and PM

Site Code : 04081423 Start Date : 4/8/2014

			High St				F	ond Street					High St			
		F	rom North					From East				F	rom South			
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysis Fro	om 07:00 AM	l to 11:45 A	M - Peak 1	of 1		_					_					
Peak Hour for Entire In	ntersection Be	egins at 08:	00 AM													
08:00 AM	0	82	18	0	100	63	0	0	0	63	0	169	0	0	169	332
08:15 AM	0	95	42	0	137	46	0	0	1	47	0	172	0	0	172	356
08:30 AM	0	82	26	0	108	72	0	0	0	72	3	182	0	0	185	365
08:45 AM	0	84	22	0	106	45	0	0	0	45	0	218	0	0	218	369
Total Volume	0	343	108	0	451	226	0	0	1	227	3	741	0	0	744	1422
% App. Total	0	76.1	23.9	0		99.6	0	0	0.4		0.4	99.6	0	0		
PHF	.000	.903	.643	.000	.823	.785	.000	.000	.250	.788	.250	.850	.000	.000	.853	.963

File Name: Pond near Nahatan AM and PM

Site Code : 04081423 Start Date : 4/8/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (near Nahatan St) 04/08/14 PM and 04/17/14 AM

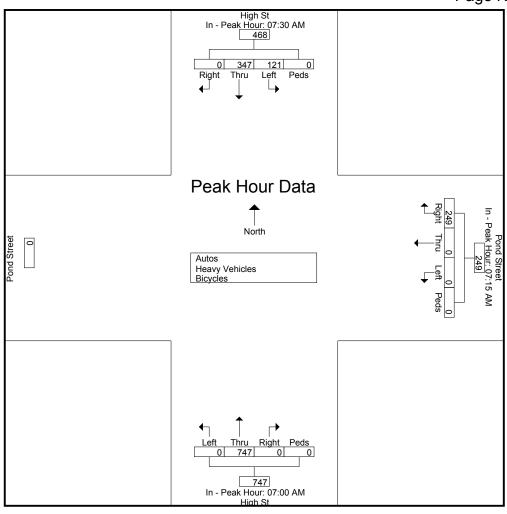
File Name: Pond near Nahatan AM and PM

Site Code : 04081423 Start Date : 4/8/2014

				High St From North				ı	Pond Street From East					High St From South			
Sta	art Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Ar	nalysis Fror	m 07:00 AM	to 11:45 A	M - Peak 1	of 1	••		•	•		••			•			
Peak Hour for	r Each App	roach Begin	ıs at:														
	0	7:30 AM					07:15 AM					07:00 AM				ļ	
+	+0 mins.	0	89	33	0	122	70	0	0	0	70	0	219	0	0	219	
+1	15 mins.	0	81	28	0	109	71	0	0	0	71	0	176	0	0	176	
+3	30 mins.	0	82	18	0	100	45	0	0	0	45	0	188	0	0	188	
+4	45 mins.	0	95	42	0	137	63	0	0	0	63	0	164	0	0	164	
Total	Volume	0	347	121	0	468	249	0	0	0	249	0	747	0	0	747	
% Ap	op. Total	0	74.1	25.9	0		100	0	0	0		0	100	0	0		
	PHF	000	913	720	000	854	877	000	000	000	877	000	853	000	000	853	İ

File Name: Pond near Nahatan AM and PM

Site Code : 04081423 Start Date : 4/8/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (near Nahatan St) 04/08/14 PM and 04/17/14 AM

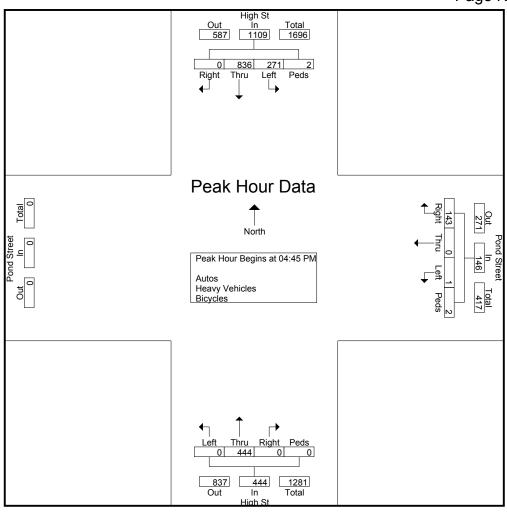
File Name: Pond near Nahatan AM and PM

Site Code : 04081423 Start Date : 4/8/2014

			High St				F	ond Street								
		F	rom North					From East								
Start Time		Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysis Fr	om 03:00 PM	I to 05:45 P	PM - Peak 1	of 1												
Peak Hour for Entire In	ntersection Be	egins at 04:	:45 PM													
04:45 PM	0	226	56	0	282	46	0	0	0	46	0	105	0	0	105	433
05:00 PM	0	195	90	1	286	35	0	1	1	37	0	117	0	0	117	440
05:15 PM	0	192	57	0	249	34	0	0	1	35	0	114	0	0	114	398
05:30 PM	0	223	68	1_	292	28	0	0	0	28	0	108	0	0	108	428
Total Volume	0	836	271	2	1109	143	0	1	2	146	0	444	0	0	444	1699
% App. Total	0	75.4	24.4	0.2		97.9	0	0.7	1.4		0	100	0	0		
PHF	.000	.925	.753	.500	.949	.777	.000	.250	.500	.793	.000	.949	.000	.000	.949	.965

File Name: Pond near Nahatan AM and PM

Site Code : 04081423 Start Date : 4/8/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (near Nahatan St) 04/08/14 PM and 04/17/14 AM

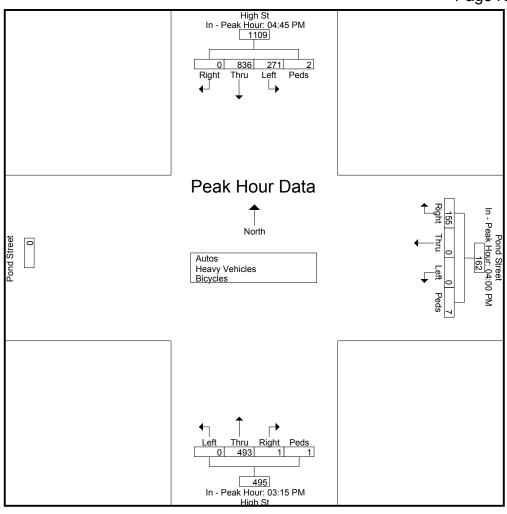
File Name: Pond near Nahatan AM and PM

Site Code : 04081423 Start Date : 4/8/2014

		F	High St From North					Pond Street From East								
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	From South Left	Peds	App. Total	Int. Total
Peak Hour Analysis F	rom 03:00 PM	to 05:45 P	M - Peak 1	of 1	•••	<u> </u>				• •	· ·					·
Peak Hour for Each A	pproach Begin	s at:														
	04:45 PM					04:00 PM					03:15 PM					ļ
+0 mins.	0	226	56	0	282	36	0	0	2	38	0	119	0	0	119	1
+15 mins.	0	195	90	1	286	36	0	0	3	39	0	126	0	0	126	
+30 mins.	0	192	57	0	249	37	0	0	2	39	1	122	0	1	124	
+45 mins.	0	223	68	1_	292	46	0	0	0	46	0	126	0	0	126	1
Total Volume	0	836	271	2	1109	155	0	0	7	162	1	493	0	1	495	ı
Mapp. Total	0	75.4	24.4	0.2		95.7	0	0	4.3		0.2	99.6	0	0.2		
PHF	000	925	753	500	949	842	000	000	583	880	250	978	000	250	982	

File Name: Pond near Nahatan AM and PM

Site Code : 04081423 Start Date : 4/8/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (Sheehan School) 04/10/14

File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014

Groups Printed- Autos - Heavy Vehicles - Bicycles High St Pond St High St Driveway														-							
			High St					Pond St					High St					Driveway			
			rom Nort					From East					om South					rom West			
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left		App. Total	Right	Thru	Left		App. Total	Right	Thru	Left		pp. Total	Int. Total
07:00 AM	1	67	2	0	70	9	0	36	0	45	75	195	0	0	270	0	0	1	0	1	386
07:15 AM	0	59	2	0	61	6	0	48	0	54	99	181	0	0	280	0	0	0	0	0	395
07:30 AM	0	89	3	0	92	5	0	49	0	54	99	185	0	0	284	0	0	0	0	0	430
07:45 AM	0	94	7	0	101	5	0	59	0	64	110	173	0	1	284	0	0	0	0	0	449
Total	1	309	14	0	324	25	0	192	0	217	383	734	0	1	1118	0	0	1	0	1	1660
08:00 AM	0	86	8	0	94	11	0	48	0	59	91	164	0	0	255	0	0	0	0	0	408
08:15 AM	0	76	5	0	81	8	0	40	0	48	94	177	0	1	272	0	0	0	0	0	401
08:30 AM	0	64	18	0	82	29	0	58	0	87	103	148	0	0	251	1	0	0	0	1	421
08:45 AM	0	77	7	0	84	26	0	38	0	64	85	175	0	1	261	0	0	0	0	0	409
Total	0	303	38	0	341	74	0	184	0	258	373	664	0	2	1039	1	0	0	0	1	1639
*** BREAK ***															,						
11:00 AM	0	87	3	0	90	7	0	36	0	43	36	94	0	1	131	0	0	0	0	0	264
11:15 AM	0	75	6	0	81	6	0	29	0	35	31	92	0	0	123	0	0	0	0	0	239
11:30 AM	0	94	4	0	98	9	0	27	0	36	25	119	0	0	144	0	0	0	0	0	278
11:45 AM	0	99	4	0	103	6	0	30	0	36	35	112	0	0	147	0	0	0	0	0	286
Total	0	355	17	0	372	28	0	122	0	150	127	417	0	1	545	0	0	0	0	0	
12:00 PM	0	110	3	0	113	8	0	35	0	43	38	118	0	0	156	0	0	0	0	0	312
12:15 PM	0	101	7	0	108	1	0	28	0	29	28	114	0	0	142	0	0	0	0	0	279
12:30 PM	0	104	4	0	108	8	0	24	0	32	38	104	0	0	142	0	0	0	0	0	282
12:45 PM	0	92	11	1	104	7	0	42	0	49	40	81	0	0	121	0	0	0	0	0	274
Total	0	407	25	1	433	24	0	129	0	153	144	417	0	0	561	0	0	0	0	0	1147
Total	Ü	407	23	1	433	24	Ü	12)	Ü	133	144	717	U	U	301	Ü	O	Ü	U	O	1147
01:00 PM	0	96	4	0	100	7	0	39	0	46	32	88	0	0	120	0	0	0	0	0	266
01:15 PM	0	89	3	0	92	10	0	40	0	50	26	79	0	2	107	0	0	0	0	0	249
01:30 PM	0	100	8	0	108	9	0	45	0	54	51	115	0	0	166	0	0	0	0	0	328
01:45 PM	0	104	6	1	111	7	0	30	0	37	49	94	0	0	143	0	0	0	0	0	291
Total	0	389	21	1	411	33	0	154	0	187	158	376	0	2	536	0	0	0	0	0	1134
*** BREAK ***																					
03:00 PM	0	141	6	0	147	10	0	60	0	70	41	108	0	0	149	0	0	0	0	0	366
03:15 PM	1	141	9	0	151	14	1	69	0	84	34	107	0	0	141	1	0	0	0	1	377
03:30 PM	2	159	4	0	165	10	0	58	0	68	40	127	1	0	168	0	0	0	0	0	401
03:45 PM	0	148	6	0	154	10	0	65	0	75	43	89	0	0	132	0	0	0	0	0	361
Total	3	589	25	0	617	44	1	252	0	297	158	431	1	0	590	1	0	0	0	1	1505
04:00 PM	1	140	11	0	152	17	0	82	2	101	50	88	0	0	138	0	0	0	0	0	391
04:00 PM 04:15 PM	0	170	7	0	177		0	82 87	2	101	30 49	88 101	0	8	158		-	0	0		439
						15				i i						0	0			0	i i
04:30 PM	1	189	10	0	200	8	0	77	0	85	52	111	0	0	163	2	0	0	0	2	450
04:45 PM	1	197	5	0	203	12	0	65		77	36	95	0	0	131	0	0	0	0	0	411
Total	3	696	33	0	732	52	0	311	4	367	187	395	0	8	590	2	0	0	0	2	1691

Central Transportation Planning Staff High St (Rte 109) at Pond St (Sheehan School) 04/10/14

File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014

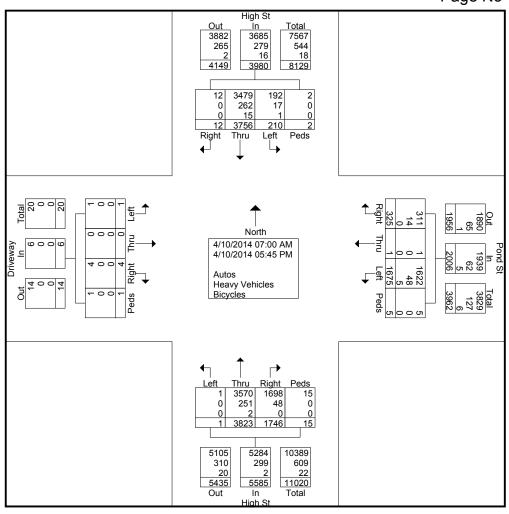
Page No : 2

Groups Printed- Autos - Heavy Vehicles - Bicycles

			High St			Pond St							High St								
		F	rom Nort	h]	From East				F	rom Sout	n			F	rom Wes	t		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
05:00 PM	5	186	15	0	206	6	0	67	0	73	59	97	0	0	156	0	0	0	1	1	436
05:15 PM	0	178	12	0	190	24	0	82	0	106	55	129	0	0	184	0	0	0	0	0	480
05:30 PM	0	187	6	0	193	5	0	82	0	87	60	91	0	0	151	0	0	0	0	0	431
05:45 PM	0	157	4	0	161	10	0	100	1	111	42	72	0	1	115	0	0	0	0	0	387
Total	5	708	37	0	750	45	0	331	1	377	216	389	0	1	606	0	0	0	1	1	1734
Grand Total	12	3756	210	2	3980	325	1	1675	5	2006	1746	3823	1	15	5585	4	0	1	1	6	11577
Apprch %	0.3	94.4	5.3	0.1		16.2	0	83.5	0.2		31.3	68.5	0	0.3		66.7	0	16.7	16.7		
Total %	0.1	32.4	1.8	0	34.4	2.8	0	14.5	0	17.3	15.1	33	0	0.1	48.2	0	0	0	0	0.1	
Autos	12	3479	192	2	3685	311	1	1622	5	1939	1698	3570	1	15	5284	4	0	1	1	6	10914
% Autos	100	92.6	91.4	100	92.6	95.7	100	96.8	100	96.7	97.3	93.4	100	100	94.6	100	0	100	100	100	94.3
Heavy Vehicles	0	262	17	0	279	14	0	48	0	62	48	251	0	0	299	0	0	0	0	0	640
% Heavy Vehicles	0	7	8.1	0	7	4.3	0	2.9	0	3.1	2.7	6.6	0	0	5.4	0	0	0	0	0	5.5
Bicycles	0	15	1	0	16	0	0	5	0	5	0	2	0	0	2	0	0	0	0	0	23
% Bicycles	0	0.4	0.5	0	0.4	0	0	0.3	0	0.2	0	0.1	0	0	0	0	0	0	0	0	0.2

File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (Sheehan School) 04/10/14

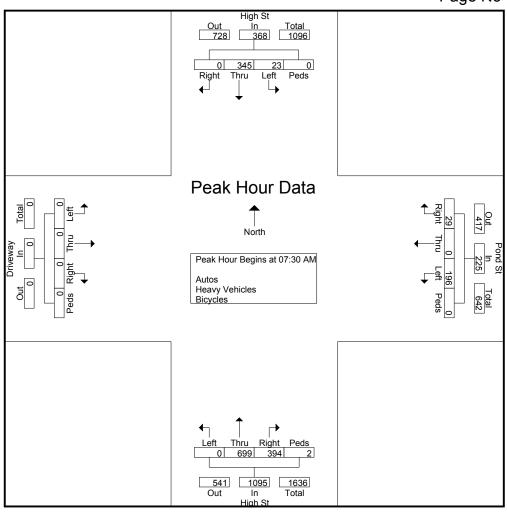
File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014

			High St			Pond St						High St						Driveway					
		F	rom Nortl	h			F	rom East	t			F	rom Sout	h			F	From Wes	t		<u> </u>		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total		
Peak Hour Analysis	From 07:0	00 AM to 0	9:45 AM	- Peak 1	of 1																		
Peak Hour for Entir	e Intersecti	on Begins	at 07:30 A	AM																			
07:30 AM	0	89	3	0	92	5	0	49	0	54	99	185	0	0	284	0	0	0	0	0	430		
07:45 AM	0	94	7	0	101	5	0	59	0	64	110	173	0	1	284	0	0	0	0	0	449		
08:00 AM	0	86	8	0	94	11	0	48	0	59	91	164	0	0	255	0	0	0	0	0	408		
08:15 AM	0	76	5	0	81	8	0	40	0	48	94	177	0	1	272	0	0	0	0	0	401		
Total Volume	0	345	23	0	368	29	0	196	0	225	394	699	0	2	1095	0	0	0	0	0	1688		
% App. Total	0	93.8	6.2	0		12.9	0	87.1	0		36	63.8	0	0.2		0	0	0	0				
PHF	.000	.918	.719	.000	.911	.659	.000	.831	.000	.879	.895	.945	.000	.500	.964	.000	.000	.000	.000	.000	.940		

File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (Sheehan School) 04/10/14

File Name: Pond near Sheehan AM+MID+PM

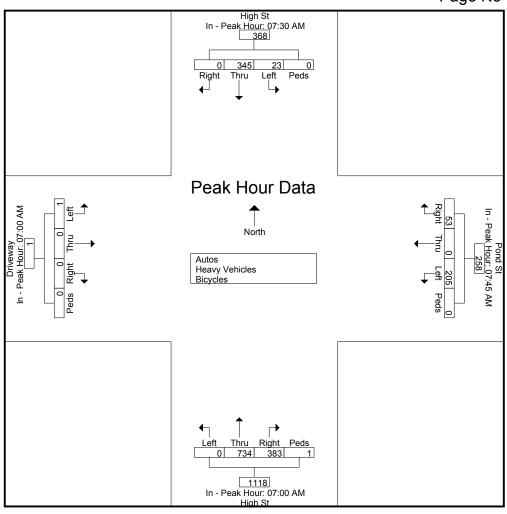
Site Code : 04101402 Start Date : 4/10/2014

Page No : 8

			High St					Pond St			High St										
		F	rom Nortl	h			I	From East	t			F	rom Soutl	1			F	rom Wes	t]
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysis	From 07:0	0 AM to 0	9:45 AM	- Peak 1	of 1	-					_					-					
Peak Hour for Each	Approach	Begins at:																			_
	07:30 AM					07:45 AM					07:00 AM					07:00 AM					1
+0 mins.	0	89	3	0	92	5	0	59	0	64	75	195	0	0	270	0	0	1	0	1	1
+15 mins.	0	94	7	0	101	11	0	48	0	59	99	181	0	0	280	0	0	0	0	0	1
+30 mins.	0	86	8	0	94	8	0	40	0	48	99	185	0	0	284	0	0	0	0	0	1
+45 mins.	0	76	5	0	81	29	0	58	0	87	110	173	0	1	284	0	0	0	0	0]
Total Volume	0	345	23	0	368	53	0	205	0	258	383	734	0	1	1118	0	0	1	0	1	1
% App. Total	0	93.8	6.2	0		20.5	0	79.5	0		34.3	65.7	0	0.1		0	0	100	0		
PHF	.000	.918	.719	.000	.911	.457	.000	.869	.000	.741	.870	.941	.000	.250	.984	.000	.000	.250	.000	.250	J

File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (Sheehan School) 04/10/14

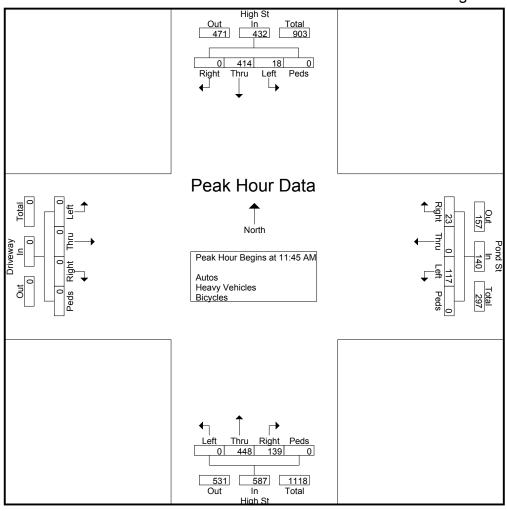
File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014

			High St					Pond St					High St					Driveway			
		F	rom Nortl	h			F	rom East				F	rom Soutl	1			F	rom West	t		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysis	From 10:0	0 AM to 0	01:45 PM	- Peak 1 c	of 1																
Peak Hour for Entire	e Intersecti	on Begins	at 11:45 A	AM																	
11:45 AM	0	99	4	0	103	6	0	30	0	36	35	112	0	0	147	0	0	0	0	0	286
12:00 PM	0	110	3	0	113	8	0	35	0	43	38	118	0	0	156	0	0	0	0	0	312
12:15 PM	0	101	7	0	108	1	0	28	0	29	28	114	0	0	142	0	0	0	0	0	279
12:30 PM	0	104	4	0	108	8	0	24	0	32	38	104	0	0	142	0	0	0	0	0	282
Total Volume	0	414	18	0	432	23	0	117	0	140	139	448	0	0	587	0	0	0	0	0	1159
% App. Total	0	95.8	4.2	0		16.4	0	83.6	0		23.7	76.3	0	0		0	0	0	0		
PHF	.000	.941	.643	.000	.956	.719	.000	.836	.000	.814	.914	.949	.000	.000	.941	.000	.000	.000	.000	.000	.929

File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (Sheehan School) 04/10/14

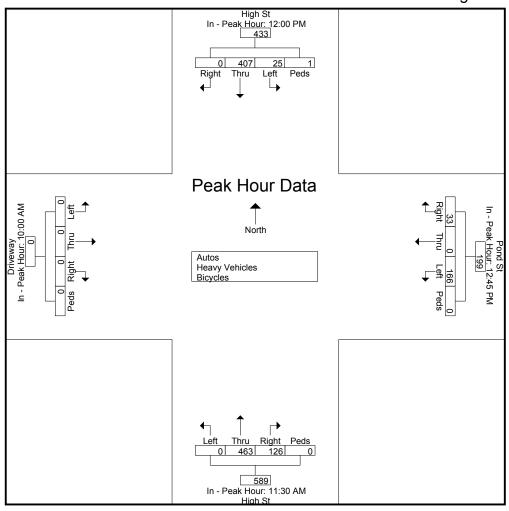
File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014

			High St					Pond St					High St					Driveway	,		
		F	rom Norti	h			F	From East	t			F	rom Soutl	ı			F	rom West	t		1
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysis	From 10:0	0 AM to 0	1:45 PM	- Peak 1	of 1	-					-										
Peak Hour for Each	Approach	Begins at:																			
	12:00 PM					12:45 PM					11:30 AM					10:00 AM					
+0 mins.	0	110	3	0	113	7	0	42	0	49	25	119	0	0	144	0	0	0	0	0	1
+15 mins.	0	101	7	0	108	7	0	39	0	46	35	112	0	0	147	0	0	0	0	0	1
+30 mins.	0	104	4	0	108	10	0	40	0	50	38	118	0	0	156	0	0	0	0	0	
+45 mins.	0	92	11	1	104	9	0	45	0	54	28	114	0	0	142	0	0	0	0	0]
Total Volume	0	407	25	1	433	33	0	166	0	199	126	463	0	0	589	0	0	0	0	0	1
% App. Total	0	94	5.8	0.2		16.6	0	83.4	0		21.4	78.6	0	0		0	0	0	0]
PHF	.000	.925	.568	.250	.958	.825	.000	.922	.000	.921	.829	.973	.000	.000	.944	.000	.000	.000	.000	.000]

File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (Sheehan School) 04/10/14

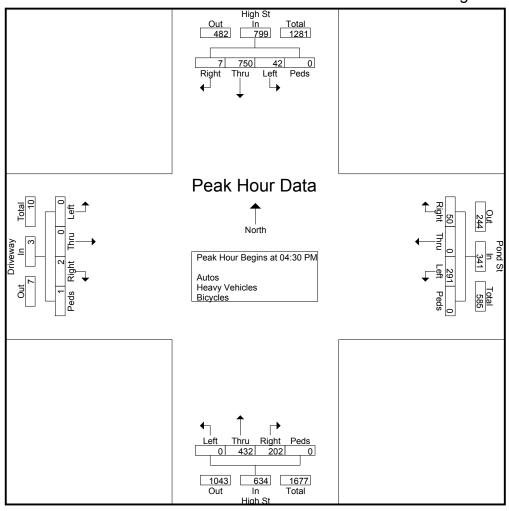
File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014

			High St					Pond St					High St					Driveway	,		
		F	rom North	1			F	rom East				F	rom Sout	1			F	rom Wes	t		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysis	From 02:0	0 PM to 0	5:45 PM -	Peak 1 o	of 1																
Peak Hour for Entire	e Intersecti	on Begins	at 04:30 I	PM																	
04:30 PM	1	189	10	0	200	8	0	77	0	85	52	111	0	0	163	2	0	0	0	2	450
04:45 PM	1	197	5	0	203	12	0	65	0	77	36	95	0	0	131	0	0	0	0	0	411
05:00 PM	5	186	15	0	206	6	0	67	0	73	59	97	0	0	156	0	0	0	1	1	436
05:15 PM	0	178	12	0	190	24	0	82	0	106	55	129	0	0	184	0	0	0	0	0	480
Total Volume	7	750	42	0	799	50	0	291	0	341	202	432	0	0	634	2	0	0	1	3	1777
% App. Total	0.9	93.9	5.3	0		14.7	0	85.3	0		31.9	68.1	0	0		66.7	0	0	33.3		
PHF	.350	.952	.700	.000	.970	.521	.000	.887	.000	.804	.856	.837	.000	.000	.861	.250	.000	.000	.250	.375	.926

File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014



Central Transportation Planning Staff High St (Rte 109) at Pond St (Sheehan School) 04/10/14

PHF

.350

.952

.700

.000

.970

.469

.000

.828

.250

File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014

Page No : 20

			High St					Pond St					High St					Driveway			
		Fr	om Nortl	h			F	From East	į			F	from South	1			F	rom Wes	t		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysis	s From 02:0	0 PM to 05	5:45 PM -	Peak 1	of 1	-					-					_					
Peak Hour for Each	Approach 1	Begins at:																			_
	04:30 PM					05:00 PM					04:30 PM					04:15 PM					
+0 mins.	1	189	10	0	200	6	0	67	0	73	52	111	0	0	163	0	0	0	0	0	
+15 mins.	1	197	5	0	203	24	0	82	0	106	36	95	0	0	131	2	0	0	0	2	
+30 mins.	5	186	15	0	206	5	0	82	0	87	59	97	0	0	156	0	0	0	0	0	
+45 mins.	0	178	12	0	190	10	0	100	1	111	55	129	0	0	184	0	0	0	1	1	
Total Volume	7	750	42	0	799	45	0	331	1	377	202	432	0	0	634	2	0	0	1	3	
% App. Total	0.9	93.9	5.3	0		11.9	0	87.8	0.3		31.9	68.1	0	0		66.7	0	0	33.3		

.849

.856

.837

.000

.000

.861

.250

.000

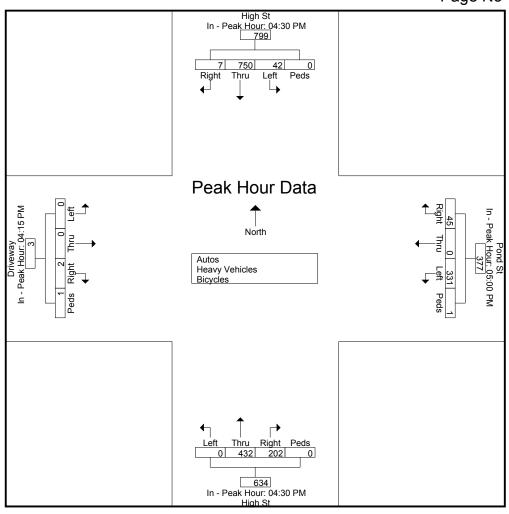
.000

.250

.375

File Name: Pond near Sheehan AM+MID+PM

Site Code : 04101402 Start Date : 4/10/2014



APPENDIX C

Crash Data



INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : Westwood				COUNT DA	TE:	4/10/2014
DISTRICT: 3	UNSIGN	ALIZED :	Х	SIGNA	LIZED :	
		~ IN	TERSECTION	I DATA ~		
MAJOR STREET :	Route 109 (H	ligh Street)				
MINOR STREET(S):	Nahatan Stre	eet, Pond Stre	eet and Rev. J	ames Coyle	Way	
INTERSECTION DIAGRAM (Label Approaches)		2 Rev James	s Coyle Way	1. High Stre	5. Nahatan S	_
			PEAK HOUF	R VOLUMES		
APPROACH:	1	2	3	4	5	Total Peak Hourly
DIRECTION:	SB	EB	NB	NWB	WB	Approach Volume
PEAK HOURLY VOLUMES (AM/PM) :	1,113	23	461	143	354	2,094
"K" FACTOR:	0.090	INTERS	ECTION ADT APPROACH	` '	AL DAILY	23,267
TOTAL # OF CRASHES :	38	# OF YEARS :	5	CRASHES	GE#OF PERYEAR():	7.80
CRASH RATE CALCU	ILATION :	0.92	RATE =	(A * 1,0	000,000) * 365)	
Comments :						
Project Title & Date:	Safety and C	perations An	alyses at Sele	cted Intersec	tionsFFY 20)14



INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : Westwood				COUNT DA	TE:	4/11/2014
DISTRICT: 3	UNSIGN	ALIZED :	Х	SIGNA	LIZED :	
		~ IN	TERSECTION	I DATA ~		
MAJOR STREET :	High Street					
MINOR STREET(S):	Pond Street					
	\uparrow			1. High Stree	et	
INTERSECTION	North					
DIAGRAM (Label Approaches)		4. Driveways	i		3. Pond Stree	et
				2. High Str	eet	
	ļ	ı	PEAK HOUF	R VOLUMES		T
APPROACH:	1	2	3	4	5	Total Peak Hourly
DIRECTION:	SB	NB	WB	EB		Approach Volume
PEAK HOURLY VOLUMES (AM/PM) :	792	634	270	2		1,698
"K" FACTOR:	0.090	INTERS	ECTION ADT APPROACH		AL DAILY	18,867
TOTAL # OF CRASHES :	9	# OF YEARS :	5	CRASHES	GE#OF PERYEAR():	1.80
CRASH RATE CALCU	ILATION :	0.26	RATE =	(A * 1,0	000,000) * 365)	
Comments :			_			
Project Title & Date:						

						Total	Total	Crash Data 2009 to	20 1Road				
	Crash	Cra	ash Crash			Nonfatal	Fatal	High Street at Nahatan Stree			Weather	Non Motorist	
ID	Number	Yea		Crash Date2	Crash Severity	Injury	Injury	Manner of Collision	Condition	Ambient Light Condition	Condition	Collision	Vehicle Action
1	L		2010 9:19 PM	1 40241	Property damage only	0	0	Angle	Wet	Dark - lighted roadway	Cloudy		V1: Travelling straight ahead / V2:Turning right
2	26070	22	2010 2:55 PM	11-May-2010	Property damage only (n	0	0	Rear-end	Dry	Daylight	Clear		V1: Slowing or stopped in traffic / V2:Slowing or sto
3	26523	05	2010 6:28 PM	04-Oct-2010	Property damage only (n	0	0	Rear-end	Wet	Dark - lighted roadway	Rain		V1: Slowing or stopped in traffic / V2:Travelling stra
4	26834	51	2011 2:34 PM	10-Jan-2011	Non-fatal injury	1	0	Single vehicle crash	Dry	Daylight	Clear	P1:Pedestrian	V1: Travelling straight ahead
5	28152	34	2011 6:44 PM	13-Nov-2011	Non-fatal injury	2	0	Rear-end	Dry	Dark - lighted roadway	Clear		V1: Slowing or stopped in traffic / V2:Travelling stra
6	5		2012 7:50 PM	07-May-2012	Non-fatal injury	0	0	Rear-end	Dry	Daylight	Clear		V1: Slowing or stopped in traffic / V2:Travelling stra
7	,		2012 5:29 PM	24-Dec-2012	Property damage only (n	0	0	Rear-end	Dry	Dark - lighted roadway	Clear		V1: Slowing or stopped in traffic / V2:Travelling stra
8	3		2013 3:39 AM	25-May-2013	Non-fatal injury	1	0	Single vehicle crash	Wet	Dark - lighted roadway	Cloudy		V1: Travelling straight ahead
9)		2013 9:07 AM	29-Oct-2013	Non-fatal injury	0	0	Sideswipe, same direction	Dry	Daylight	Rain		V1: Travelling straight ahead / V2:Travelling straigh
10	24781	89	2009 11:06 AM	04-Jun-2009	Property damage only (n	0	0	Rear-end	Dry	Daylight	Clear		V1: Entering traffic lane / V2:Entering traffic lane
11	25945	27	2009 4:00 PM	24-Aug-2009	Non-fatal injury	1	0	Rear-end	Dry	Daylight	Clear		V1: Entering traffic lane / V2:Entering traffic lane
12	25946	48	2010 9:04 PM	16-Feb-2010	Property damage only (n	0	0	Single vehicle crash	Snow	Dark - lighted roadway	Snow		V1: Turning left
13	3		2013 4:31 PM	16-Oct-2013	Property damage only (n	0	0	Single vehicle crash	Dry	Daylight	Clear		V1: Travelling straight ahead
14	24554	19	2009 4:07 PM	08-Apr-2009	Property damage only (n	0	0	Sideswipe, same direction	Dry	Daylight	Cloudy		V1: Travelling straight ahead / V2:Entering traffic la
15	24710	63	2009 9:33 PM	15-May-2009	Non-fatal injury	2	0	Rear-end	Dry	Dark - lighted roadway	Clear		V1: Entering traffic lane / V2:Entering traffic lane
16	25946	77	2010 2:14 PM	22-Mar-2010	Property damage only (n	0	0	Rear-end	Wet	Daylight	Rain		V1: Travelling straight ahead / V2:Travelling straigh
17	25946	86	2010 9:14 AM	14-Apr-2010	Property damage only (n	0	0	Sideswipe, same direction	Dry	Daylight	Clear		V1: Changing lanes / V2:Travelling straight ahead
18	26000	78	2010 10:42 AM	07-May-2010	Property damage only (n	0	0	Angle	Dry	Daylight	Clear		V1: Turning left / V2:Turning left
19	26299	55	2010 8:22 AM	10-Aug-2010	Property damage only (n	0	0	Angle	Dry	Daylight	Clear		V1: Overtaking/passing / V2:Turning left
20	26523	09	2010 8:05 AM	13-Oct-2010	Property damage only (n	0	0	Single vehicle crash	Dry	Daylight	Clear		V1: Travelling straight ahead / V2:Travelling straigh
21	26624	71	2010 5:15 PM	08-Nov-2010	Property damage only (n	0	0	Angle	Wet	Dark - lighted roadway	Rain		V1: Turning left / V2:Travelling straight ahead
22	27166	42	2011 12:54 PM	18-Apr-2011	Property damage only (n	0	0	Sideswipe, same direction	Dry	Daylight	Clear		V1: Turning right / V2:Travelling straight ahead
23	27400	02	2011 9:41 AM	24-Jun-2011	Property damage only (n	0	0	Rear-end	Wet	Daylight	Cloudy		V1: Travelling straight ahead / V2:Slowing or stoppe
24	26492	63	2010 2:08 PM	02-Oct-2010	Property damage only (n	0	0	Sideswipe, same direction	Dry	Daylight	Clear		V1: Travelling straight ahead / V2:Travelling straigh
25	27506	36	2011 5:42 PM	28-Jul-2011	Property damage only (n	0	0	Angle	Dry	Daylight	Clear		V1: Turning left / V2:Travelling straight ahead
26	5		2012 6:44 PM	01-Mar-2012	Property damage only (n	0	0	Rear-end	Snow	Dark - lighted roadway	Snow		V1: Travelling straight ahead / V2:Travelling straigh
27	7		2012 9:32 PM	23-Apr-2012	Property damage only (n	0	0	Sideswipe, same direction	Dry	Dark - lighted roadway	Clear		V1: Changing lanes / V2:Travelling straight ahead
28	3		2012 8:50 AM	21-May-2012	Property damage only (n	0	0	Angle	Wet	Daylight	Rain		V1: Turning left / V2:Travelling straight ahead
29)		2012 2:24 PM	24-May-2012	Property damage only (n	0	0	Rear-end	Dry	Daylight	Clear		V1: Turning right / V2:Turning right
30)		2012 2:49 PM	17-Sep-2012	Property damage only (n	0	0	Rear-end	Dry	Daylight	Clear		V1: Turning right / V2:Turning right
31			2012 7:34 AM	21-Sep-2012	Property damage only (n	0	0	Rear-end	Dry	Daylight	Clear		V1: Turning right / V2:Turning right
32	2		2012 5:44 PM	10-Dec-2012	Property damage only (n	0	0	Angle	Wet	Dark - lighted roadway	Rain		V1: Turning left / V2:Turning left
33	3		2013 6:44 AM	19-Mar-2013	Property damage only (n	0	0	Rear-end	Snow	Daylight	Snow		V1: Slowing or stopped in traffic / V2:Travelling stra
34			2013 11:00 AM	15-Nov-2013	Non-fatal injury	1	0	Angle	Dry	Daylight	Clear		V1: Travelling straight ahead / V2:Travelling straigh
35	5		2013 1:03 PM		Non-fatal injury	1	0	Rear-end	Dry	Daylight	Clear		V1: Entering traffic lane / V2:Travelling straight ahe
36	5		2013 8:36 AM	09-Aug-2013	Property damage only (n	0	0	Single vehicle crash	Dry	Daylight	Clear		V1: Travelling straight ahead
37	7		2011 5:42 PM	28-Jul-2011	Property damage only (n	0	0	Angle	Dry	Daylight	Clear		V1: Turning left / V2:Travelling straight ahead
38	3		2010 2:08 PM	02-Oct-2010	Property damage only (n	0	0	Sideswipe, same direction	Dry	Daylight	Clear		V1: Travelling straight ahead / V2:Travelling straigh
39)		2010 11:13 PM	10-Feb-2010	Property damage only (n	0	0	Single vehicle crash	Snow	Dark - lighted roadway	Snow		V1: Travelling straight ahead

Crash Data 2009 to 2013 High Street at Pond Street (near Sheehan School)

						Total	Total					
	Crash	Crash	Crash			Nonfatal	Fatal		Road		Weather	
ID	Number	Year	Time	Crash Date	Crash Severity	Injury	Injury	Manner of Collision	Surface	Ambient Light	Condition	Vehicle Action
1	2444033	2009	9:51 AM	05-Mar-2009	Property damage only (no	0	0	Angle	Dry	Daylight	Clear	V1: Travelling straight ahead / V2:Turning left
2	2646813	2010	4:14 PM	18-Sep-2010	Property damage only (no	0	0	Angle	Dry	Daylight	Cloudy	V1: Turning left / V2:Turning left
3	2702033	2011	3:08 PM	04-Mar-2011	Property damage only (no	0	0	Angle	Dry	Daylight	Clear	V1: Turning left / V2:Turning left
4	2789517	2011	6:47 PM	06-Oct-2011	Property damage only (no	0	0	Single vehicle crash	Dry	Dark - lighted roadway	Clear	V1: Travelling straight ahead / V2:Travelling straight ah
5		2012	7:43 AM	14-May-2012	Property damage only (no	0	0	Angle	Wet	Daylight	Rain	V1: Turning right / V2:Travelling straight ahead
6		2012	12:23 PM	28-Nov-2012	Property damage only (no	0	0	Angle	Dry	Daylight	Cloudy	V1: Turning left / V2:Turning left
7		2013	4:07 PM	02-Feb-2013	Property damage only (no	0	0	Angle	Dry	Daylight	Clear	V1: Travelling straight ahead / V2:Turning left
8		2013	8:30 PM	17-Apr-2013	Property damage only (no	0	0	Angle	Dry	Dark - lighted roadway	Clear	V1: Turning right / V2:Travelling straight ahead
9	2612528	2010	8:15 AM	10-Jun-2010	Property damage only (no	0	0	Angle	Dry	Daylight	Cloudy	V1: Turning right / V2:Travelling straight ahead

APPENDIX D

Level of Service Analysis

Intersection												
	9.4											
in belay, siven	7.1											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Vol, veh/h	0	707	313	245	374	5	95	2	187	2	1	2
Conflicting Peds, #/hr	0	0	5	0	0	5	10	0	107	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop		Stop	Stop	Stop	Stop
RT Channelized	1166	1166	Free	-	-	None	3ιυμ	Stop	Yield	310p	Siup -	None
Storage Length		-	-	250	-	-	-	-	150	-	-	INOTIC
Veh in Median Storage, #	_	0	_	230	0	_	_	1	130	_	1	_
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90
Heavy Vehicles, %	3	3	3	3	3	3	3	3	3	3	3	3
Mymt Flow	0	786	348	272	416	6	106	2	208	2	1	2
IVIVIIIL FIOW	U	700	340	212	410	U	100	Z	200	2	ļ	Z
Major/Minor	Major1			Major2			Minor1			Minor2		
Conflicting Flow All	421	0		796	0	0	1760	1762	408	1367	1759	418
Stage 1	421	-	-	190	-	-	796	796	400	963	963	410
	-	-	-	-	-	-	790 964	966	-	404	796	-
Stage 2 Critical Hdwy	4.13	-	-	4.16	-	-	7.345					6.245
J	4.13			4.10	-		6.545			6.145		0.243
Critical Edwy Stg 1	-	-	-	-	-	-		5.545	-		5.545	-
Critical Hdwy Stg 2 Follow-up Hdwy	2.227	-	-	2.23	-	-	3.5285		2 2205	3.5285		- 2 220E
. ,	1133	-	-	815	-	-	3.5285 ~ 59	4.0285	591		4.0285 84	3.3285 631
Pot Cap-1 Maneuver	1133	-	0	813	-		~ 59 346	396		114	331	031
Stage 1	-	-	0	-	-	-	346		-	305		-
Stage 2	-	-	0	-	-	-	304	330	-	593	396	-
Platoon blocked, %	1122	-		012	-	-	42	55	584	ГА	ГГ	/ 21
Mov Cap-1 Maneuver	1133	-	-	812	-	-	~ 43			54	55	631
Mov Cap-2 Maneuver	-	-	-	-	-	-	133	151	-	89	93	-
Stage 1	-	-	-	-	-	-	343	393	-	305	220	-
Stage 2	-	-	-	-	-	-	200	219	-	378	393	-
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			4.6			42.8			32.4		
HCM LOS							E			D		
Minor Lane/Major Mvmt	NBLn1 I	NBLn2	EBL	EBT WBL	WBT	WBR S	BLn1					
Capacity (veh/h)	133	584	1133	- 812	-	-	137					
HCM Lane V/C Ratio	0.81	0.356	-	- 0.335	-	-	0.041					
HCM Control Delay (s)	97.5	14.5	0	- 11.7	-	-	32.4					
HCM Lane LOS	F	В	A	- B	-	-	D					
HCM 95th %tile Q(veh)	5	1.6	0	- 1.5	-	-	0.1					
Notes												
	ity ¢. D.	alay aya	eeds 30)Oc Com	nutatio	n Not De	ofined *. Al	l major :	volumo	in platoon		
~: Volume exceeds capac	ity \$: De	ciay exc	.eeus 3(JUS +: COM	μαιαιίθ	I NOLDE	iiileu : Al	ппаји	volulile	in platoon		

Movement Vol, veh/h Conflicting Peds, #/hr	EBL													
Vol, veh/h		EBT	EBR		WBL	WBT	WBR		NBL	NBT	NBR	SBL	SBT	SBI
	9	497	98		210	940	2		148	1	205	2	1	301
	10	0	10		0	0	0		140	0	10	10	0	10
Sign Control	Free	Free	Free		Free	Free	Free		Stop	Stop	Stop	Stop	Stop	Sto
RT Channelized	1100	-	Free		-	-	None		Stop	Stop	Yield	5100	Stop	None
Storage Length	_	_	-		250	_	-			_	150	_	-	INOIN
Veh in Median Storage, #		0	-		-	0	-			1	-	-	1	
Grade, %	_	0	_		_	0	_		_	0	_	-	0	
Peak Hour Factor	96	96	96		96	96	96		96	96	96	96	96	9
Heavy Vehicles, %	3	3	3		3	3	3		3	3	3	3	3	
Mymt Flow	9	518	102		219	979	2		154	1	214	2	1	
With Flow	,	010	102		217	,,,	_		101		211	_		Í
Major/Minor	Major1			[Major2				Minor1			Minor2		
Conflicting Flow All	991	0	-		528	0	0		1975	1975	269	1716	1974	1000
Stage 1	-	-	-		-	-	-		546	546	-	1428	1428	
Stage 2	-	-	-		-	-	-		1429	1429	-	288	546	
Critical Hdwy	4.13	-	-		4.16	-	-		5.3	5.3	5.5	7.345	6.545	6.245
Critical Hdwy Stg 1	-	-	-		-	-	-		5.3	5.3	-	6.145	5.545	
Critical Hdwy Stg 2	-	-	-		-	-	-		5.3	5.3	-	6.545	5.545	
Follow-up Hdwy	2.227	-	-		2.23	-	-			4.0285	3.3285	3.5285	4.0285	3.3285
Pot Cap-1 Maneuver	694	-	0		1028	-	-		~ 145	121	810	64	61	292
Stage 1	-	-	0		-	-	-		774	535	-	166	198	
Stage 2	-	-	0		-	-	-		277	218	-	694	515	
Platoon blocked, %		-				-	-							
Mov Cap-1 Maneuver	688	-	-		1028	-	-		~ 116	92	803	38	46	287
Mov Cap-2 Maneuver	-	-	-		-	-	-		176	138	-	110	110	
Stage 1	-	-	-		-	-	-		754	521	-	162	155	
Stage 2	-	-	-		-	-	-		213	170	-	499	502	
Annroach	EB				WB				NB			SB		
Approach	0.3				1.7				45.5			30.6		
HCM Control Delay, s	0.3				1.7				45.5 E					
HCM LOS									E			D		
Minor Lane/Major Mvmt	NBLn1	NBLn2	EBL	EBT	WBL	WBT	WBR	SBLn1						
Capacity (veh/h)	176	803	688	-	1028		-	146						
HCM Lane V/C Ratio	0.882	0.266	0.014	-	0.213	-	-	0.036						
HCM Control Delay (s)	92.8	11.1	10.3	0.1	9.4		-	30.6						
HCM Lane LOS	72.8 F	В	В	A	A	-	-	D						
HCM 95th %tile Q(veh)	6.4	1.1	0	-	0.8	-	-	0.1						

+: Computation Not Defined

*: All major volume in platoon

~: Volume exceeds capacity

\$: Delay exceeds 300s

Intersection												
	11.2											
in Doiay Gron												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Vol, veh/h	0	710	315	245	375	5	95	5	190	2	1	2
Conflicting Peds, #/hr	0	0	5	0	0	5	10	0	10	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	Free	-	-	None	-	-	Yield	-	-	None
Storage Length	_	_	-	250	_	-	_	-	0	_	-	-
Veh in Median Storage, #	‡ -	0	_	-	0	_	_	1	-	-	1	_
Grade, %	_	0	_	-	0	_	_	0	_	_	0	_
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90
Heavy Vehicles, %	3	3	3	3	3	3	3	3	3	3	3	3
Mvmt Flow	0	813	360	280	429	6	109	6	217	2	1	2
		0.0	000	200	,				,	_	•	_
Major/Minor	Major1			Major2			Minor1			Minor2		
Conflicting Flow All	435	0		823	0	0	1818	1819	421	1412	1816	432
Stage 1	430	-	_	023	-	-	823	823	421	993	993	432
Stage 2	-	<u>-</u>	-	-	-	-	995	996	-	419	823	-
Critical Hdwy	4.13	-	_	4.16	_	-	7.345	6.545			6.545	6 2/15
Critical Hdwy Stg 1	4.13		-	4.10	-			5.545	0.743	6.145		0.243
Critical Hdwy Stg 2	-	_	-	-	-	-		5.545	-	6.545		-
Follow-up Hdwy	2.227	-	-	2.23	-		3.5285			3.5285		2 2285 -
Pot Cap-1 Maneuver	1119	_	0	796	_	_	~ 54	4.0203 77	580	106	4.0203 77	620
Stage 1	-		0	770	_		333	385	J00 -	293	321	020
Stage 2	_	_	0	_	_	_	292	320	_	581	385	
Platoon blocked, %		_	U		_	_	272	320		301	303	
Mov Cap-1 Maneuver	1119	_	_	793	_	_	~ 38	49	573	46	49	620
Mov Cap-2 Maneuver	-	_	_	-	_	_	125	143	-	65	81	020
Stage 1	_	_	_	_	_	_	330	382	_	293	208	
Stage 2	_	_	_	_	_	_	187	207	_	354	382	_
Stage 2							107	201		334	302	
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			4.7			52.3			40.2		
	U			4.7			52.3 F			40.2 E		
HCM LOS							Г			E		
Minor Long /Maior M. mat	NDI 1 N	ייי וחו	EDI	EDT WOL	WDT	WDD C	DI1					
Minor Lane/Major Mvmt	NBLn1 N		EBL	EBT WBL	WBT	WBR S						
Capacity (veh/h)	126	573	1119	- 793	-	-	108					
HCM Control Dalay (a)	0.908		-	- 0.354	-		0.053					
HCM Long LOS	123	15.1	0	- 12	-	-	40.2					
HCM Lane LOS	F	C	A	- B	-	-	E					
HCM 95th %tile Q(veh)	5.9	1.8	0	- 1.6	-	-	0.2					
Notes												
~: Volume exceeds capa	city \$: De	elay exc	eeds 30	00s +: Com	putation	n Not De	fined *: All	major	volume	in platoon		

Intersection												
	41.4											
·												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NE	L NBT	NBR	SBL	SBT	SBR
Vol, veh/h	9	497	98	210	940	2	15	0 5	205	2	1	2
Conflicting Peds, #/hr	10	0	10	0	0	0	1	0 0	10	10	0	10
Sign Control	Free	Free	Free	Free	Free	Free	Sto	p Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	Free	-	-	None		•	Yield	<u>.</u>	'-	None
Storage Length	-	-	-	250	-	-			- 0	-	-	_
Veh in Median Storage,	# -	0	-	-	0	-		- 1		-	1	
Grade, %	-	0	-	-	0	-		- (-	0	_
Peak Hour Factor	96	96	96	96	96	96	Ç	6 96		96	96	96
Heavy Vehicles, %	3	3	3	3	3	3		2 2		0	0	0
Mvmt Flow	10	533	105	225	1009	2	16			2	1	2
	.,	000			.007	_				_	•	_
Major/Minor	Major1			Major2			Mino	1		Minor2		
Conflicting Flow All	1021	0		543	0	0	203		277	1769	2033	1030
Stage 1	1021	-	_	J4J -	-	-	56			1470	1470	1030
Stage 2		_			_		147			299	563	_
Critical Hdwy	4.13	-		4.16		_	7.3			7.3	6.5	6.2
Critical Hdwy Stg 1	4.13	-	-	4.10		-	6.5			6.1	5.5	0.2
Critical Hdwy Stg 2			_	_	_	_	6.1			6.5	5.5	_
Follow-up Hdwy	2.227	_	_	2.23	_		3.51			3.5	4	3.3
Pot Cap-1 Maneuver	676		0	1015		_	~ 3			60	58	286
Stage 1	-		0	1013	_		47			160	193	200
Stage 2	-	-	0	-		_	~ 15			691	512	_
Platoon blocked, %	-	-	U	-	-	-	~ 10	/ 170	, -	071	312	-
Mov Cap-1 Maneuver	670	-	_	1015	-	-	~ 2	9 43	715	32	43	281
Mov Cap-2 Maneuver	-	-	-	1015	-	-	~ 2			100	105	201
•	-	_	-	-	_	-	46			155	149	_
Stage 1	-	-	-	-	-	-	40 ~ 11			463	497	-
Stage 2	-	-	-	-	-	-	~ 11	9 147	-	403	497	-
A	ED.			WD			NI	n		CD		
Approach	EB			WB			N			SB		
HCM Control Delay, s	0.3			1.7			226			32.6		
HCM LOS								F		D		
Minor Lane/Major Mvmt	NBLn1 N		EBL	EBT WBL	WBT	WBR S						
Capacity (veh/h)	89	715	670	- 1015	-	-	136					
HCM Lane V/C Ratio		0.308	0.014	- 0.222	-	- (0.039					
HCM Control Delay (s)	\$ 509.6	12.3	10.5	0.1 9.6	-	-	32.6					
HCM Lane LOS	F	В	В	A A	-	-	D					
HCM 95th %tile Q(veh)	14.1	1.3	0	- 0.8	-	-	0.1					
Notes												
~: Volume exceeds capa	city \$: De	elay exc	ceeds 30	00s +: Com	putatio	n Not De	fined *:	All major	volume	in platoon		
•	•	-						•		•		

Intersection												
	7.7											
J.												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Vol, veh/h	0	707	313	245	374	5	95	2	187	2	1	2
Conflicting Peds, #/hr	0	0	5	0	0	5	10	0	10	0	0	C
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	Yield	-	-	None	<u>.</u>	<u>'</u> -	Free	<u>.</u>	'-	None
Storage Length	-	-	0	250	-	-	-	-	0	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	1	-	-	1	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90
Heavy Vehicles, %	3	3	3	3	3	3	3	3	3	3	3	3
Mvmt Flow	0	809	358	280	428	6	109	2	214	2	1	2
Major/Minor	Major1			Major2			Minor1			Minor2		
Conflicting Flow All	434	0	0	819	0	0	1812	1814		1812	1811	436
Stage 1	-	-	-	-	-	-	819	819	_	992	992	-
Stage 2	-	_	_	_		_	993	995	_	820	819	-
Critical Hdwy	4.13	_	_	4.13	_	_	7.13	6.53	_	7.13	6.53	6.23
Critical Hdwy Stg 1	-	_	_	-		_	6.13	5.53	_	6.13	5.53	0.20
Critical Hdwy Stg 2	_	_	_	_	_	_	6.13	5.53	_	6.13	5.53	_
Follow-up Hdwy	2.227	_	_	2.227	_	_	3.527	4.027	_	3.527	4.027	3.327
Pot Cap-1 Maneuver	1120	_	_	805	_	_	~ 60	78	0	60	78	618
Stage 1	-	_	_	-	_	_	368	388	0	295	322	-
Stage 2	_	_	_	_	_	_	294	321	0	368	388	_
Platoon blocked, %		_	_		_	_	27.	021		000	000	
Mov Cap-1 Maneuver	1115	_	-	802	_	-	~ 43	50	_	43	50	615
Mov Cap-2 Maneuver	-	_	_	-	_	_	131	144	_	71	83	-
Stage 1	_	_	_	_	_	_	365	385	_	295	210	_
Stage 2	-	_	_	-	_	-	189	209	_	364	385	_
otago z							107			001	000	
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			4.7			106.1			37.9		
HCM LOS	U			4.7			F			57.7 E		
TICIVI LOS										L		
Minor Lane/Major Mvmt	NBLn1 N	IDI no	EBL	EBT EBR	WBL	WBT	WBR SBLn1					
Capacity (veh/h)	131	NDLIIZ	1115		802	-	- 115					
HCM Lane V/C Ratio	0.847	-	-		0.35		0.05					
HCM Control Delay (s)	106.1	0			11.9	-	07.0					
HCM Lane LOS	106.1 F	A	0 A			-	-					
HCM 95th %tile Q(veh)	5.3	- A	0		1.6		- E					
	0.3	_	U		1.0	-	- 0.2					
Notes												
~: Volume exceeds capac	city \$: De	lay exc	eeds 30	00s +: Com	putation	n Not D	efined *: All	major v	olume i	n platoon		

Int Delay, s/veh	Intersection												
Vol, veh/h Conflicting Peds, #/hr O O 0 F F F F F F F F F F F F F F F F F		46.1											
Vol, veh/h Conflicting Peds, #/hr O O 0 F F F F F F F F F F F F F F F F F													
Conflicting Peds, #hr	Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Sign Control Free Free Free Free Free Free Free Free Stop Stop Stop Stop Stop Stop Stop Storage Length None Free None Free None Free None None Free None	Vol, veh/h	0	497	98	210	940	2	148	1	205	2	1	2
Sign Control Free Free Free Free Free Free Free Free Stop Stop Stop Stop Stop Stor Storago S		0	0	5	0	0	5	10	0	10	0	0	(
RT Channelized		Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
Veh in Median Storage, # - 0 0 1 1 1 Grade, % - 0 - 0 0 - 0 1 - 0 - 0 - 0 -	RT Channelized	-	-	Yield	-	-	None	•	•		•	•	None
Veh in Median Storage, # - 0 0 1 1 1 Grade, % - 0 - 0 0 - 0 1 - 0 - 0 - 0 -	Storage Length	-	-	0	250	-	-	-	-	0	-	-	
Grade, % - 0 0 0 0 0 0 0 Peak Hour Factor 90 90 90 90 90 90 90 90 90 90 90 90 90	o o	ŧ -	0	-	-	0	-	-	1	-	-	1	
Peak Hour Factor 90 90 90 90 90 90 90 90 90 90 90 90 90	Grade, %		0	-	-	0	-	-		-	-		
Heavy Vehicles, % 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	Peak Hour Factor	90	90	90	90	90	90	90	90	90	90		90
Mymit Flow 0 569 112 240 1076 2 169 1 235 2 1 Major/Minor Major I Major 2 Minor 1 Minor 2 Conflicting Flow All 1078 0 0 579 0 2138 2138 2137 2137 108 Stage 1 - - - - - - 579 579 - 1558 1558 Stage 2 - - - - - 1559 1559 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579 579	Heavy Vehicles, %	3	3	3	3	3	3	3	3	3	3	3	3
Conflicting Flow All 1078 0 0 579 0 0 2138 2138 - 2137 2137 108. Stage 1 579 579 - 1558 1558 Stage 1 579 579 - 1558 1558 Stage 2 1559 1559 1559 - 579 579 579 Critical Hdwy 4.13 4.13 1559 1559 - 579 579 579 Critical Hdwy Stg 1 6.13 5.53 - 6.13 5.53 Critical Hdwy Stg 1 6.13 5.53 - 6.13 5.53 Critical Hdwy Stg 2 6.13 5.53 - 6.13 5.53 Follow-up Hdwy 2.227 2.227 3.527 4.027 - 3.527 4.027 3.52 Pot Cap-1 Maneuver 643 990 35 49 0 35 49 26 Stage 1 499 499 0 140 172 Stage 2 499 499 0 140 172 Stage 2 104 172 0 499 499 Poly Poly Doublocked, % Follow-up Hdwu 640 986 28 37 - 28 37 26. Mov Cap-1 Maneuver 640 986 28 37 - 28 37 26. Mov Cap-2 Maneuver 640 986 28 37 - 28 37 26. Mov Cap-2 Maneuver 640 986 28 5 104 - 94 93 Stage 1 104 130 - 496 495 Poly Doublocked 7	Mvmt Flow	0	569	112	240	1076	2	169	1		2		2
Conflicting Flow All 1078 0 0 579 0 0 2138 2138 - 2137 2137 108. Stage 1 579 579 - 1558 1558 Stage 1 579 579 - 1558 1558 Stage 2 1559 1559 1559 - 579 579 579 Critical Hdwy 4.13 4.13 1559 1559 - 579 579 579 Critical Hdwy Stg 1 6.13 5.53 - 6.13 5.53 Critical Hdwy Stg 1 6.13 5.53 - 6.13 5.53 Critical Hdwy Stg 2 6.13 5.53 - 6.13 5.53 Follow-up Hdwy 2.227 2.227 3.527 4.027 - 3.527 4.027 3.52 Pot Cap-1 Maneuver 643 990 35 49 0 35 49 26 Stage 1 499 499 0 140 172 Stage 2 499 499 0 140 172 Stage 2 104 172 0 499 499 Poly Poly Doublocked, % Follow-up Hdwu 640 986 28 37 - 28 37 26. Mov Cap-1 Maneuver 640 986 28 37 - 28 37 26. Mov Cap-2 Maneuver 640 986 28 37 - 28 37 26. Mov Cap-2 Maneuver 640 986 28 5 104 - 94 93 Stage 1 104 130 - 496 495 Poly Doublocked 7													
Conflicting Flow All 1078 0 0 579 0 0 2138 2138 - 2137 2137 108. Stage 1 579 579 - 1558 1558 Stage 1 579 579 - 1558 1558 Stage 2 1559 1559 1559 - 579 579 579 Critical Hdwy 4.13 4.13 1559 1559 - 579 579 579 Critical Hdwy Stg 1 6.13 5.53 - 6.13 5.53 Critical Hdwy Stg 1 6.13 5.53 - 6.13 5.53 Critical Hdwy Stg 2 6.13 5.53 - 6.13 5.53 Follow-up Hdwy 2.227 2.227 3.527 4.027 - 3.527 4.027 3.52 Pot Cap-1 Maneuver 643 990 35 49 0 35 49 26 Stage 1 499 499 0 140 172 Stage 2 499 499 0 140 172 Stage 2 104 172 0 499 499 Poly Poly Doublocked, % Follow-up Hdwu 640 986 28 37 - 28 37 26. Mov Cap-1 Maneuver 640 986 28 37 - 28 37 26. Mov Cap-2 Maneuver 640 986 28 37 - 28 37 26. Mov Cap-2 Maneuver 640 986 28 5 104 - 94 93 Stage 1 104 130 - 496 495 Poly Doublocked 7	Maior/Minor	Maior1			Maior2			Minor1			Minor2		
Stage 1			0	0		0	0		2138			2137	1082
Stage 2		1070											1002
Critical Hdwy Stg 1		_											
Critical Howy Stg 1	Ü		_				_						6.23
Critical Hdwy Stg 2	J		_				_						0.23
Follow-up Hdwy 2.227 - 2.227 - 3.527 4.027 - 3.527 4.027 3.32 Pot Cap-1 Maneuver 643 - 99035 49 0 35 49 26 Stage 1 499 499 0 140 172 Stage 2 499 499 0 140 172 Platoon blocked, % Mov Cap-1 Maneuver 640 - 986 28 37 - 28 37 26 Mov Cap-2 Maneuver 495 495 - 140 130 Stage 1 495 495 - 140 130 Stage 1 495 495 - 140 130 Stage 2 495 495 - 140 130 Stage 2 104 130 - 496 495 Approach EB WB NB SB HCM Control Delay, s 0 1.8 \$572.9 34.9 HCM LOS F D Minor Lane/Major Mvmt NBLn1 NBLn2 EBL EBT EBR WBL WBT WBR SBLn1 Capacity (veh/h) 85 - 640 - 986 - 126 HCM Lane V/C Ratio 2.006 0.244 - 0.045 HCM Control Delay (s) \$572.9 0 0 - 9.8 - 34.9 HCM Lane LOS F A A - A - D HCM 95th %tile Q(veh) 15 - 0 - 1 - 0.1 Notes													
Pot Cap-1 Maneuver 643 - 990 - - 35 49 0 35 49 26 Stage 1 - - - - - 499 499 0 140 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172 172													3 3 3 7 7
Stage 1	. ,												
Stage 2													200
Platoon blocked, % Mov Cap-1 Maneuver 640 986 28 37 - 28 37 26. Mov Cap-2 Maneuver 85 104 - 94 93 Stage 1 495 495 - 140 130 Stage 2 104 130 - 496 495 Approach EB WB NB SB HCM Control Delay, s 0 1.8 \$572.9 34.9 HCM LOS F D Minor Lane/Major Mvmt NBLn1 NBLn2 EBL EBT EBR WBL WBT WBR SBLn1 Capacity (veh/h) 85 - 640 - 986 - 126 HCM Lane V/C Ratio 2.006 0.244 - 0.045 HCM Control Delay (s) \$572.9 0 0 - 9.8 - 34.9 HCM Lane LOS F A A - A - D HCM 95th %tile Q(veh) 15 - 0 - 1 - 0.1 Notes		_	_										
Mov Cap-1 Maneuver 640 - - 986 - - 28 37 - 28 37 26 Mov Cap-2 Maneuver - - - - - - 85 104 - 94 93 Stage 1 - - - - - 495 495 - 140 130 Stage 2 - - - - - - - - 104 130 - 496 495 Approach EB WB WB NB SB - - 496 495 - - - - 104 130 - 496 495 - - - - - - 104 495 - - - - - - - - - - - - - - - - - - - -								7 170	172	U	7//	7//	
Mov Cap-2 Maneuver - - - - 85 104 - 94 93 Stage 1 - - - - 495 495 - 140 130 Stage 2 - - - - 104 130 - 496 495 Approach EB WB NB NB SB HCM Control Delay, s 0 1.8 \$572.9 34.9 HCM LOS F D D Minor Lane/Major Mvmt NBLn1 NBLn2 EBL EBT EBR WBL WBT WBR SBLn1 Capacity (veh/h) 85 - 640 - 986 - 126 HCM Lane V/C Ratio 2.006 0.244 - 0.045 HCM Control Delay (s) \$572.9 0 0 - 9.8 - 34.9 HCM Lane LOS F A A - A - D HCM 95th %tile Q(veh) 15 - 0 - 1 - 0.1 Notes HCM 2004		640			086			- 28	27	_	28	37	262
Stage 1 - - - - - - 495 495 - 140 130 Stage 2 - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -	•												202
Stage 2	•	-	-				-						-
Approach EB WB NB SB HCM Control Delay, s 0 1.8 \$572.9 34.9 HCM LOS F D Minor Lane/Major Mvmt NBLn1 NBLn2 EBL EBT EBR WBL WBT WBR SBLn1 Capacity (veh/h) 85 - 640 - 986 - 126 HCM Lane V/C Ratio 2.006 0.244 - 0.045 HCM Control Delay (s) \$572.9 0 0 - 9.8 - 34.9 HCM Lane LOS F A A - A - B - D HCM 95th %tile Q(veh) 15 - 0 - 1 - 0.1 Notes		-	-			-	-						-
HCM Control Delay, s 0 1.8 \$572.9 34.9 HCM LOS F D Minor Lane/Major Mvmt NBLn1 NBLn2 EBL EBT EBR WBL WBT WBR SBLn1 Capacity (veh/h) 85 - 640 986 126 HCM Lane V/C Ratio 2.006 0.244 - 0.045 HCM Control Delay (s) \$572.9 0 0 - 9.8 - 34.9 HCM Lane LOS F A A - A - D HCM 95th %tile Q(veh) 15 - 0 - 1 - 0.1	Staye 2	-	-	-	-	-	-	~ 104	130	-	470	473	-
HCM Control Delay, s 0 1.8 \$572.9 34.9 HCM LOS F D Minor Lane/Major Mvmt NBLn1 NBLn2 EBL EBT EBR WBL WBT WBR SBLn1 Capacity (veh/h) 85 - 640 986 126 HCM Lane V/C Ratio 2.006 0.244 - 0.045 HCM Control Delay (s) \$572.9 0 0 - 9.8 - 34.9 HCM Lane LOS F A A - A - D HCM 95th %tile Q(veh) 15 - 0 - 1 - 0.1	Annragah	רח			WD			ND			CD		
Minor Lane/Major Mvmt NBLn1 NBLn2 EBL EBT EBR WBL WBT WBR SBLn1													
Minor Lane/Major Mvmt NBLn1 NBLn2 EBL EBT EBR WBL WBT WBR SBLn1 Capacity (veh/h) 85 - 640 - - 986 - - 126 HCM Lane V/C Ratio 2.006 - - - 0.244 - - 0.045 HCM Control Delay (s) \$ 572.9 0 0 - - 9.8 - - 34.9 HCM Lane LOS F A A - - A - D HCM 95th %tile Q(veh) 15 - 0 - - 1 - 0.1		0			1.8								
Capacity (veh/h) 85 - 640 - 986 - 126 HCM Lane V/C Ratio 2.006 0.244 - 0.045 HCM Control Delay (s) \$ 572.9 0 0 - 9.8 - 34.9 HCM Lane LOS FAAA - A - D A - D HCM 95th %tile Q(veh) 15 - 0 - 1 - 1 - 0.1 Notes - 0.1	HCM LOS							F			D		
Capacity (veh/h) 85 - 640 - 986 - 126 HCM Lane V/C Ratio 2.006 0.244 - 0.045 HCM Control Delay (s) \$ 572.9 0 0 - 9.8 - 34.9 HCM Lane LOS FAAA - A - D A - D HCM 95th %tile Q(veh) 15 - 0 - 1 - 1 - 0.1 Notes - 0.1													
HCM Lane V/C Ratio 2.006 0.244 0.045 HCM Control Delay (s) \$ 572.9 0 0 - 9.8 - 34.9 HCM Lane LOS F A A - A - D HCM 95th %tile Q(veh) 15 - 0 - 1 - 0.1			IBLn2				WBT						
HCM Control Delay (s) \$ 572.9 0 0 9.8 34.9 HCM Lane LOS F A A A D HCM 95th %tile Q(veh) 15 - 0 1 0.1			-	640			-						
HCM Lane LOS F A A - - A - - D HCM 95th %tile Q(veh) 15 - 0 - - 1 - - 0.1 Notes							-						
HCM 95th %tile Q(veh) 15 - 0 1 0.1 Notes							-						
Notes			Α				-						
	HCM 95th %tile Q(veh)	15	-	0		1	-	- 0.1					
~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon	Notes												
	~: Volume exceeds capa	city \$: De	lay exc	eeds 30	00s +: Com	putation	n Not D	efined *: All	major v	volume i	n platoon		

Intersection												
	11.2											
in Doiay Gron												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Vol, veh/h	0	710	315	245	375	5	95	5	190	2	1	2
Conflicting Peds, #/hr	0	0	5	0	0	5	10	0	10	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	Free	-	-	None	-	-	Yield	-	-	None
Storage Length	_	_	-	250	_	-	_	-	0	_	-	-
Veh in Median Storage, #	‡ -	0	_	-	0	_	_	1	-	-	1	_
Grade, %	_	0	_	-	0	-	_	0	_	_	0	_
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90
Heavy Vehicles, %	3	3	3	3	3	3	3	3	3	3	3	3
Mvmt Flow	0	813	360	280	429	6	109	6	217	2	1	2
		0.0	000	200	,				,	_	•	_
Major/Minor	Major1			Major2			Minor1			Minor2		
Conflicting Flow All	435	0		823	0	0	1818	1819	421	1412	1816	432
Stage 1	430	-	_	023	-	-	823	823	421	993	993	432
Stage 2	-	<u>-</u>	-	-	-	-	995	996	-	419	823	-
Critical Hdwy	4.13	-	_	4.16	_	-	7.345	6.545			6.545	6 2/15
Critical Hdwy Stg 1	4.13		-	4.10	-			5.545	0.743	6.145		0.243
Critical Hdwy Stg 2	-	_	-	-	-	-		5.545	-	6.545		-
Follow-up Hdwy	2.227	-	-	2.23	-		3.5285			3.5285		2 2285 -
Pot Cap-1 Maneuver	1119	_	0	796	_	_	~ 54	4.0203 77	580	106	4.0203 77	620
Stage 1	-		0	770	_		333	385	J00 -	293	321	020
Stage 2	_	_	0	_	_	_	292	320	_	581	385	
Platoon blocked, %		_	U		_	_	272	320		301	303	
Mov Cap-1 Maneuver	1119	_	_	793	_	_	~ 38	49	573	46	49	620
Mov Cap-2 Maneuver	-	_	_	-	_	_	125	143	-	65	81	020
Stage 1	_	_	_	_	_	_	330	382	_	293	208	
Stage 2	_	_	_	_	_	_	187	207	_	354	382	_
Stage 2							107	201		334	302	
Approach	EB			WB			NB			SB		
HCM Control Delay, s	0			4.7			52.3			40.2		
	U			4.7			52.3 F			40.2 E		
HCM LOS							Г			E		
Minor Long /Maior M. mat	NDI 1 N	ייי וחו	EDI	EDT WOL	WDT	WDD C	DI1					
Minor Lane/Major Mvmt	NBLn1 N		EBL	EBT WBL	WBT	WBR S						
Capacity (veh/h)	126	573	1119	- 793	-	-	108					
HCM Control Dalay (a)	0.908		-	- 0.354	-		0.053					
HCM Long LOS	123	15.1	0	- 12	-	-	40.2					
HCM Lane LOS	F	C	A	- B	-	-	E					
HCM 95th %tile Q(veh)	5.9	1.8	0	- 1.6	-	-	0.2					
Notes												
~: Volume exceeds capa	city \$: De	elay exc	eeds 30	00s +: Com	putation	n Not De	fined *: All	major	volume	in platoon		

Intersection												
	41.4											
·												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NE	L NBT	NBR	SBL	SBT	SBR
Vol, veh/h	9	497	98	210	940	2	15	0 5	205	2	1	2
Conflicting Peds, #/hr	10	0	10	0	0	0	1	0 0	10	10	0	10
Sign Control	Free	Free	Free	Free	Free	Free	Sto	p Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	Free	-	-	None		•	Yield	<u>.</u>	'-	None
Storage Length	-	-	-	250	-	-			- 0	-	-	_
Veh in Median Storage,	# -	0	-	-	0	-		- 1		-	1	
Grade, %	-	0	-	-	0	-		- (-	0	_
Peak Hour Factor	96	96	96	96	96	96	Ç	6 96		96	96	96
Heavy Vehicles, %	3	3	3	3	3	3		2 2		0	0	0
Mvmt Flow	10	533	105	225	1009	2	16			2	1	2
	.,	000			.007	_				_	•	_
Major/Minor	Major1			Major2			Mino	1		Minor2		
Conflicting Flow All	1021	0		543	0	0	203		277	1769	2033	1030
Stage 1	1021	-	_	J4J -	-	-	56			1470	1470	1030
Stage 2		_			_		147			299	563	_
Critical Hdwy	4.13	-		4.16		_	7.3			7.3	6.5	6.2
Critical Hdwy Stg 1	4.13	-	-	4.10		-	6.5			6.1	5.5	0.2
Critical Hdwy Stg 2			_	_	_	_	6.1			6.5	5.5	_
Follow-up Hdwy	2.227	_	_	2.23	_		3.51			3.5	4	3.3
Pot Cap-1 Maneuver	676		0	1015		_	~ 3			60	58	286
Stage 1	-		0	1013	_		47			160	193	200
Stage 2	-	-	0	-		_	~ 15			691	512	_
Platoon blocked, %	-	-	U	-	-	-	~ 10	/ 170	, -	071	312	-
Mov Cap-1 Maneuver	670	-	_	1015	-	-	~ 2	9 43	715	32	43	281
Mov Cap-2 Maneuver	-	-	-	1015	-	-	~ 2			100	105	201
•	-	_	-	-	_	-	46			155	149	_
Stage 1	-	-	-	-	-	-	40 ~ 11			463	497	-
Stage 2	-	-	-	-	-	-	~ 11	9 147	-	403	497	-
A	ED.			WD			NI	n		CD		
Approach	EB			WB			N			SB		
HCM Control Delay, s	0.3			1.7			226			32.6		
HCM LOS								F		D		
Minor Lane/Major Mvmt	NBLn1 N		EBL	EBT WBL	WBT	WBR S						
Capacity (veh/h)	89	715	670	- 1015	-	-	136					
HCM Lane V/C Ratio		0.308	0.014	- 0.222	-	- (0.039					
HCM Control Delay (s)	\$ 509.6	12.3	10.5	0.1 9.6	-	-	32.6					
HCM Lane LOS	F	В	В	A A	-	-	D					
HCM 95th %tile Q(veh)	14.1	1.3	0	- 0.8	-	-	0.1					
Notes												
~: Volume exceeds capa	city \$: De	elay exc	ceeds 30	00s +: Com	putatio	n Not De	fined *:	All major	volume	in platoon		
•	•	-						•		•		

	۶	→	•	•	+	•	1	†	/	/	+	4
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		€Î.Þ		¥	ĵ.			ની	7		4	
Volume (vph)	0	710	315	245	375	5	95	5	190	2	1	2
Satd. Flow (prot)	0	3311	0	1752	1840	0	0	1762	1568	0	1710	0
Flt Permitted				0.111				0.734			0.883	
Satd. Flow (perm)	0	3311	0	205	1840	0	0	1330	1525	0	1541	0
Satd. Flow (RTOR)					1						2	
Adj. Flow (vph)	0	813	360	280	429	6	109	6	217	2	1	2
Lane Group Flow (vph)	0	1173	0	280	435	0	0	115	217	0	5	0
Turn Type		NA		pm+pt	NA		Perm	NA	pm+ov	Perm	NA	
Protected Phases		2		1	6			8	1		4	
Permitted Phases	2			6			8		8	4		
Total Split (s)	41.0	41.0		15.0	56.0		21.0	21.0	15.0	21.0	21.0	
Total Lost Time (s)		5.0		5.0	5.0			5.0	5.0		5.0	
Act Effct Green (s)		36.1		51.8	53.3			11.4	19.8		11.0	
Actuated g/C Ratio		0.49		0.70	0.72			0.15	0.27		0.15	
v/c Ratio		0.72		0.77	0.33			0.56	0.52		0.02	
Control Delay		21.6		32.2	8.3			43.4	22.2		27.0	
Queue Delay		0.0		0.0	0.0			0.0	0.0		0.0	
Total Delay		21.6		32.2	8.3			43.4	22.2		27.0	
LOS		С		С	Α			D	С		С	
Approach Delay		21.6			17.7			29.6			27.0	
Approach LOS		С			В			С			С	
Queue Length 50th (ft)		202		61	61			48	70		1	
Queue Length 95th (ft)		#536		#308	251			127	114		12	
Internal Link Dist (ft)		226			305			1179			272	
Turn Bay Length (ft)				250					150			
Base Capacity (vph)		1696		364	1333			302	417		352	
Starvation Cap Reductn		0		0	0			0	0		0	
Spillback Cap Reductn		0		0	0			0	0		0	
Storage Cap Reductn		0		0	0			0	0		0	
Reduced v/c Ratio		0.69		0.77	0.33			0.38	0.52		0.01	

Intersection Summary

Cycle Length: 100

Actuated Cycle Length: 73.6

Control Type: Actuated-Uncoordinated Maximum v/c Ratio: 0.77

Intersection Signal Delay: 21.5
Intersection Capacity Utilization 75.7%

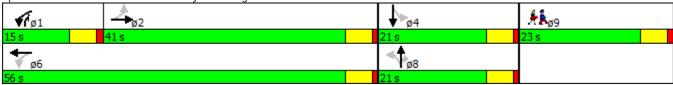
Intersection LOS: C
ICU Level of Service D

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Nahatan St/Rev Coyle Cir & High St



	۶	→	•	•	+	•	•	†	/	/	Ţ	4
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		નીક		Ť	ą.			ર્ન	7		4	
Volume (vph)	10	500	90	210	940	5	150	5	205	2	1	2
Satd. Flow (prot)	0	3402	0	1752	1843	0	0	1760	1568	0	1690	0
Flt Permitted		0.861		0.289				0.729			0.900	
Satd. Flow (perm)	0	2932	0	533	1843	0	0	1321	1568	0	1544	0
Satd. Flow (RTOR)												
Adj. Flow (vph)	11	536	97	225	1009	5	161	5	220	2	1	2
Lane Group Flow (vph)	0	644	0	225	1014	0	0	166	220	0	5	0
Turn Type	Perm	NA		pm+pt	NA		Perm	NA	pt+ov	Perm	NA	
Protected Phases		2		1	6			8	8 1		4	
Permitted Phases	2			6			8			4		
Total Split (s)	34.0	34.0		13.0	47.0		20.0	20.0		20.0	20.0	
Total Lost Time (s)		5.0		5.0	5.0			5.0			5.0	
Act Effct Green (s)		29.8		42.8	42.8			13.1	25.4		13.1	
Actuated g/C Ratio		0.43		0.61	0.61			0.19	0.36		0.19	
v/c Ratio		0.51		0.48	0.90			0.67	0.39		0.02	
Control Delay		18.6		12.6	26.9			43.0	16.4		26.6	
Queue Delay		0.0		0.0	0.0			0.0	0.0		0.0	
Total Delay		18.6		12.6	26.9			43.0	16.4		26.6	
LOS		В		В	С			D	В		С	
Approach Delay		18.6			24.3			27.8			26.6	
Approach LOS		В			С			С			С	
Queue Length 50th (ft)		94		33	287			61	59		2	
Queue Length 95th (ft)		227		124	#933			#191	98		12	
Internal Link Dist (ft)		256			298			1197			272	
Turn Bay Length (ft)				250					150			
Base Capacity (vph)		1251		469	1131			289	546		338	
Starvation Cap Reductn		0		0	0			0	0		0	
Spillback Cap Reductn		0		0	0			0	0		0	
Storage Cap Reductn		0		0	0			0	0		0	
Reduced v/c Ratio		0.51		0.48	0.90			0.57	0.40		0.01	

Intersection Summary

Cycle Length: 90

Actuated Cycle Length: 69.7

Control Type: Actuated-Uncoordinated Maximum v/c Ratio: 0.90

Intersection Signal Delay: 23.3
Intersection Capacity Utilization 96.9%

Intersection LOS: C
ICU Level of Service F

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Nahatan St/Rev Coyle Cir & High St



MOVEMENT SUMMARY



Site: High St at Nahatan St AM

Single Lane Roundabout Roundabout

Move	ment Perfo	rmance - Ve	hicles						_		
Mov	OD	Demand		Deg.	Average	Level of	95% Back		Prop.	Effective	Average
ID	Mov	Total	HV	Satn	Delay	Service	Vehicles	Distance	Queued	Stop Rate	Speed
South	: High St	veh/h	%	v/c	sec		veh	ft		per veh	mph
3	L2	1	3.0	0.961	45.1	LOS E	21.4	548.8	1.00	1.31	21.2
8	T1	777	3.0	0.961	45.1	LOS E	21.4	548.8	1.00	1.31	21.2
-	R2	345			_					0.00	
18			3.0	0.212	0.0	LOSA	0.0	0.0	0.00		36.5
Appro	ach	1123	3.0	0.961	31.3	LOS D	21.4	548.8	0.69	0.91	24.3
East: I	Nahatan St										
1	L2	104	3.0	0.309	16.2	LOS C	1.3	33.3	0.76	0.77	27.7
6	T1	5	0.0	0.309	16.2	LOS C	1.3	33.3	0.76	0.77	27.8
16	R2	208	2.0	0.127	0.0	LOS A	0.0	0.0	0.00	0.00	36.5
Appro	ach	318	2.3	0.309	5.6	LOSA	1.3	33.3	0.26	0.26	32.8
North:	High St										
7	L2	268	3.0	0.358	7.6	LOS A	2.0	51.5	0.37	0.22	31.2
4	T1	410	3.0	0.358	7.6	LOS A	2.0	51.5	0.37	0.22	32.5
14	R2	5	3.0	0.358	7.6	LOS A	2.0	51.5	0.37	0.22	32.0
Appro	ach	683	3.0	0.358	7.6	LOSA	2.0	51.5	0.37	0.22	32.0
West:	Rev Coyle C	ir									
5	L2	2	0.0	0.011	7.7	LOS A	0.0	0.9	0.59	0.50	31.9
2	T1	1	0.0	0.011	7.7	LOSA	0.0	0.9	0.59	0.50	32.0
12	R2	2	0.0	0.011	7.7	LOS A	0.0	0.9	0.59	0.50	31.4
Appro	ach	5	0.0	0.011	7.7	LOSA	0.0	0.9	0.59	0.50	31.7
All Vel	nicles	2129	2.9	0.961	19.8	LOS C	21.4	548.8	0.52	0.59	27.5

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: US HCM 2010.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Processed: Monday, September 15, 2014 1:10:34 PM SIDRA INTERSECTION 6.0.24.4877

Copyright © 2000-2014 Akcelik and Associates Pty Ltd www.sidrasolutions.com

Project: C:\13261_Safety_and_Operations_Analyses_Selected_Intersections_FFY2014\Westwood\Synchro

\Roundabout Single Lane.sip6 8001137, 6016968, CTPS, PLUS / 1PC



MOVEMENT SUMMARY



Site: High St at Nahatan St PM

Single Lane Roundabout Roundabout

Move	ment Perfo	ormance - Ve	hicles								
Mov	OD	Demand		Deg.	Average	Level of	95% Back		Prop.	Effective	Average
ID	Mov	Total	HV	Satn	Delay	Service	Vehicles	Distance	Queued	Stop Rate	Speed
South:	High St	veh/h	%	v/c	sec		veh	ft		per veh	mph
3	L2	11	0.0	0.827	29.7	LOS D	8.3	213.6	0.90	1.10	24.8
8	T1	547	3.0	0.827	29.7	LOS D	8.3	213.6	0.90	1.10	24.8
18	R2	99	3.0	0.061	0.0	LOSA	0.0	0.0	0.00	0.00	36.5
Approa	ach	657	2.9	0.827	25.3	LOS D	8.3	213.6	0.76	0.94	26.0
East: N	Nahatan St										
1	L2	165	3.0	0.275	9.4	LOS A	1.0	25.9	0.58	0.58	30.1
6	T1	5	0.0	0.275	9.4	LOS A	1.0	25.9	0.58	0.58	30.3
16	R2	224	3.0	0.138	0.0	LOSA	0.0	0.0	0.00	0.00	36.5
Approa	ach	394	3.0	0.275	4.1	LOSA	1.0	25.9	0.25	0.25	33.4
North:	High St										
7	L2	230	3.0	0.694	15.6	LOS C	6.2	155.6	0.65	0.54	28.7
4	T1	1028	3.0	0.694	15.9	LOS C	6.2	155.6	0.64	0.53	29.0
14	R2	5	0.0	0.694	16.1	LOS C	5.7	147.9	0.62	0.52	28.6
Approa	ach	1264	3.0	0.694	15.9	LOS C	6.2	155.6	0.64	0.53	29.0
West:	Rev Coyle C	Cir									
5	L2	2	0.0	0.020	14.2	LOS B	0.1	1.5	0.77	0.77	29.3
2	T1	1	0.0	0.020	14.2	LOS B	0.1	1.5	0.77	0.77	29.4
12	R2	2	0.0	0.020	14.2	LOS B	0.1	1.5	0.77	0.77	28.8
Approa	ach	5	0.0	0.020	14.2	LOS B	0.1	1.5	0.77	0.77	29.1
All Veh	nicles	2320	3.0	0.827	16.5	LOS C	8.3	213.6	0.61	0.60	28.7

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: US HCM 2010.

HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

Gap-Acceptance Capacity: Traditional M1.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Processed: Monday, September 15, 2014 1:14:39 PM SIDRA INTERSECTION 6.0.24.4877

Copyright © 2000-2014 Akcelik and Associates Pty Ltd www.sidrasolutions.com

Project: C:\13261_Safety_and_Operations_Analyses_Selected_Intersections_FFY2014\Westwood\Synchro \Roundabout Single Lane.sip6

8001137, 6016968, CTPS, PLUS / 1PC



Intersection							
	17.8						
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
Vol, veh/h	700	400	25	345	196		
Conflicting Peds, #/hr	700	400	0	0	0	0	
sign Control	Free	Free	Free	Free	Stop		
RT Channelized	-	Free	-	Free	310p	None	
Storage Length	-	-		1166	50		
/eh in Median Storage, #		-	-	0	0	U	
Grade, %	0	-	-	0	0	-	
Peak Hour Factor	94	94	94	94	94	94	
leavy Vehicles, %	4	4	4	4	2		
Ivmt Flow	745	426	27	367	209	32	
WITH FIOW	740	420	21	307	209	32	
lajor/Minor	Major1		Major2		Minor1		
Conflicting Flow All	0	-	745	0	1165	745	
Stage 1	-	-	-	-	745	-	
Stage 2	-	-	-	-	420	-	
critical Hdwy	-	-	4.14	-	6.42	6.22	
ritical Hdwy Stg 1	-	-	-	-	5.42	-	
ritical Hdwy Stg 2	-	-	-	-	5.42	-	
ollow-up Hdwy	-	-	2.236	-	3.518	3.318	
ot Cap-1 Maneuver	-	0	854	-	215	414	
Stage 1	-	0	-	-	469	-	
Stage 2	-	0	-	-	663	-	
latoon blocked, %	-			-			
lov Cap-1 Maneuver	-	-	854	-	~ 206	414	
lov Cap-2 Maneuver	-	-	-	-	~ 206	-	
Stage 1	-	-	-	-	469	-	
Stage 2	-	-	-	-	636	-	
oproach	EB		WB		NB		
CM Control Delay, s	0		0.6		101.2		
CM LOS	U		0.0		F		
CIVI LUS					Г		
inor Lane/Major Mvmt	NBLn1 NBLn2	EBT	WBL WBT				
apacity (veh/h)	206 414	-	854 -				
CM Lane V/C Ratio	1.012 0.077	- (0.031 -				
CM Control Delay (s)	114.5 14.4	-	9.4 0				
CM Lane LOS	F B	-	A A				
CM 95th %tile Q(veh)	9 0.2	-	0.1 -				
otes							
Volume exceeds capa	city \$: Delay exc	oods 20	ns L. Com	nutation	Not Defined *: Al	I major volume	in platoon
volume exceeds capa	city a. Delay ext	ccus 30	us +. Culli	pulaliUH	i Not Dellineu : Al	i major volume	iii pialuull

Intersection							
nt Delay, s/veh 28.6	,)						
2 5.ag / 6/15 25.5							
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
Vol, veh/h	435	200	45	760	290	50	
Conflicting Peds, #/hr	0	200	0	0	0	0	
ign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	Free	-	Free	- Jiop	None	
Storage Length	_	-	_	-	50	0	
eh in Median Storage, #	0	_	_	0	0	-	
Grade, %	0	_	_	0	0	_	
eak Hour Factor	94	94	94	94	94	94	
eavy Vehicles, %	4	4	4	4	2	2	
lvmt Flow	463	213	48	809	309	53	
aior/Minor	Major1		Majora		Minor1		
ajor/Minor	Major1		Major2	^	Minor1	4/0	
Conflicting Flow All	0	-	463	0	1367	463	
Stage 1	-	-	-	-	463	-	
Stage 2	-	-	-	-	904	-	
ritical Hdwy	-	-	4.14	-	5.3	5.3	
ritical Hdwy Stg 1	-	-	-	-	5.42	-	
itical Hdwy Stg 2	-	-	- 2.227	-	5.42	-	
ollow-up Hdwy	-	-	2.236	-	2.7	2.7	
ot Cap-1 Maneuver	-	0	1088	-	~ 285	798	
Stage 1	-	0	-	-	786	-	
Stage 2	-	0	-	-	471	-	
atoon blocked, %	-		1000	-	2/2	700	
ov Cap-1 Maneuver	-	-	1088	-	~ 262	798	
ov Cap-2 Maneuver	-	-	-	-	~ 262	-	
Stage 1	-	-	-	-	786	-	
Stage 2	-	-	-	-	433	-	
pproach	EB		WB		NB		
CM Control Delay, s	0		0.5		131.9		
CM LOS					F		
linor Lane/Major Mvmt	NBLn1 NBLn2	EBT	WBL WBT				
apacity (veh/h)	262 798		1088 -				
CM Lane V/C Ratio	1.178 0.067		0.044 -				
CM Control Delay (s)	152.9 9.8	- (8.5 0				
CM Lane LOS	F A	-	A A				
CM 95th %tile Q(veh)	14 0.2	-	0.1 -				
	11 0.2		0.1				
otes							
: Volume exceeds capacity	\$: Delay exc	eeds 30	0s +: Com	putation	Not Defined *: All	major volume i	n platoon

23.5						
FBT	FBR	WBI	WBT	NBI	NBR	
				-	-	
				- Jiop	•	
			-	50		
	_	_	0		-	
	_	_			-	
		94			94	
707	100	21	370	217	33	
	-	767			767	
-	-	-	-		-	
-	-	-	-		-	
-	-	4.14	-		6.22	
-	-	-	-		-	
-	-	-	-		-	
-	-		-			
-		838	-		402	
-		-	-		-	
-	0	-	-	654	-	
-			-			
-	-	838	-		402	
-	-	-	-		-	
-	-	-	-		-	
-	-	-	-	627	-	
EB		WB		NB		
		0.0				
				•		
NDI1 NDI2	EDT	WDI WDT				
	-					
	-					
	-					
10.6 0.3	-	0.1 -				
	- - - - - - - - -	EBT EBR 700 400 0 2 Free Free - Free - Free - -	EBT EBR WBL 700 400 25 0 2 0 0 0 0 0 0 0 0	EBT EBR WBL WBT	FBT EBR WBL WBT NBL	FBT FBR WBL WBT NBL NBR

Intersection							
	34.8						
							
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
/ol, veh/h	435	200	45	750	290	50	
onflicting Peds, #/hr	0	200	0	0	0	0	
gn Control	Free	Free	Free	Free	Stop	Stop	
T Channelized	-	Free	-	Free	310p	None	
orage Length	-	-	_	-	50	0	
eh in Median Storage, #		_	_	0	0	-	
rade, %	0	_	_	0	0	_	
eak Hour Factor	94	94	94	94	94	94	
eavy Vehicles, %	4	4	4	4	2	2	
mt Flow	477	219	49	822	318	55	
			.,	022	0.0		
oior/Minor	Major1		Major2		Minor1		
ajor/Minor	Major1 0	_	Major2 477	0	1397	477	
onflicting Flow All					477	4//	
Stage 1	-	-	-	-		-	
Stage 2	-	-	4.14	-	920 5.3	5.3	
itical Hdwy	-	-	4.14	-	5.3	5.3	
itical Hdwy Stg 1	-	-	-	-	5.42	-	
ritical Hdwy Stg 2	-		2.236	-	2.7	2.7	
ollow-up Hdwy ot Cap-1 Maneuver	-	0	1075	-	~ 275	786	
Stage 1	<u> </u>	0	1073	-	773	700	
Stage 2	-	0	-	_	462	-	
atoon blocked, %		U	-	-	402	-	
ov Cap-1 Maneuver	-	_	1075	-	~ 252	786	
ov Cap-1 Maneuver			1075	-	~ 252	700	
Stage 1	-			_	773	-	
Stage 2					423		
Stage 2					423		
	- F5		LA /ID		HD		
oproach	EB		WB		NB 150.7		
CM Control Delay, s	0		0.5		159.7		
CM LOS					F		
nor Lane/Major Mvmt	NBLn1 NBLn2	EBT W	/BL WBT				
apacity (veh/h)	252 786	- 10	075 -				
CM Lane V/C Ratio	1.261 0.07	- 0.0	046 -				
CM Control Delay (s)	185.5 9.9	-	8.5 0				
CM Lane LOS	F A	-	A A				
CM 95th %tile Q(veh)	15.8 0.2	-	0.1 -				
otes							
Volume exceeds capac	tity \$: Delay exc	oods 200	L. Com	nutation	Not Defined *: All	major volume	in platoon
volume exceeds capac	ny a. Delay exc	ccus 3005	+. Culli	pulaliUH	NOL DEILIEU : All	major volume	ווו טומנטטוו

	۶	→	•	•	+	•	1	†	<i>></i>	/	+	4
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		*	7	7			ř	ĥ			4	
Volume (vph)	0	700	400	25	345	0	200	0	30	2	2	2
Satd. Flow (prot)	0	1827	1553	1736	1827	0	1770	1583	0	0	1750	0
Flt Permitted				0.173			0.754				0.939	
Satd. Flow (perm)	0	1827	1519	316	1827	0	1405	1583	0	0	1670	0
Satd. Flow (RTOR)			228					414			2	
Adj. Flow (vph)	0	767	438	27	378	0	219	0	33	2	2	2
Lane Group Flow (vph)	0	767	438	27	378	0	219	33	0	0	6	0
Turn Type		NA	Perm	Perm	NA		Perm	NA		Perm	NA	
Protected Phases		2			6			8			4	
Permitted Phases			2	6			8			4		
Total Split (s)		50.0	50.0	50.0	50.0		17.0	17.0		17.0	17.0	
Total Lost Time (s)		5.0	5.0	5.0	5.0		5.0	5.0			5.0	
Act Effct Green (s)		32.4	32.4	32.4	32.4		12.8	12.8			12.8	
Actuated g/C Ratio		0.55	0.55	0.55	0.55		0.22	0.22			0.22	
v/c Ratio		0.76	0.47	0.16	0.38		0.72	0.05			0.02	
Control Delay		18.0	6.1	11.2	9.8		42.6	0.1			24.2	
Queue Delay		0.0	0.0	0.0	0.0		0.0	0.0			0.0	
Total Delay		18.0	6.1	11.2	9.8		42.6	0.1			24.2	
LOS		В	Α	В	Α		D	Α			С	
Approach Delay		13.7			9.9			37.1			24.2	
Approach LOS		В			Α			D			С	
Queue Length 50th (ft)		147	27	3	53		65	0			1	
Queue Length 95th (ft)		#590	145	26	198		#290	0			13	
Internal Link Dist (ft)		548			727			534			42	
Turn Bay Length (ft)			100	75			50					
Base Capacity (vph)		1467	1265	254	1467		306	668			365	
Starvation Cap Reductn		0	0	0	0		0	0			0	
Spillback Cap Reductn		0	0	0	0		0	0			0	
Storage Cap Reductn		0	0	0	0		0	0			0	
Reduced v/c Ratio		0.52	0.35	0.11	0.26		0.72	0.05			0.02	

Intersection Summary

Cycle Length: 90

Actuated Cycle Length: 58.9

Control Type: Actuated-Uncoordinated Maximum v/c Ratio: 0.76

Intersection Signal Delay: 16.0 Intersection Capacity Utilization 64.4%

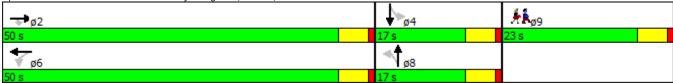
Intersection LOS: B ICU Level of Service C

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Pond St /Driveway & High St (Rte 109)



	۶	→	\rightarrow	•	•	•	1	†	/	>	ļ	4
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		*	7	7	ĵ.		ř	ĵ.			₩	
Volume (vph)	0	430	200	45	750	5	290	1	50	2	2	2
Satd. Flow (prot)	0	1827	1553	1736	1825	0	1770	1589	0	0	1750	0
Flt Permitted				0.388			0.754				0.951	
Satd. Flow (perm)	0	1827	1553	709	1825	0	1405	1589	0	0	1692	0
Satd. Flow (RTOR)			161					55			2	
Adj. Flow (vph)	0	471	219	49	822	5	318	1	55	2	2	2
Lane Group Flow (vph)	0	471	219	49	827	0	318	56	0	0	6	0
Turn Type		NA	Prot	Perm	NA		Perm	NA		Perm	NA	
Protected Phases		2	2		6			8			4	
Permitted Phases				6			8			4		
Total Split (s)		43.0	43.0	43.0	43.0		24.0	24.0		24.0	24.0	
Total Lost Time (s)		5.0	5.0	5.0	5.0		5.0	5.0			5.0	
Act Effct Green (s)		38.5	38.5	38.5	38.5		19.3	19.3			19.3	
Actuated g/C Ratio		0.54	0.54	0.54	0.54		0.27	0.27			0.27	
v/c Ratio		0.48	0.24	0.13	0.84		0.84	0.12			0.01	
Control Delay		14.2	4.6	12.1	26.1		48.5	8.8			20.8	
Queue Delay		0.0	0.0	0.0	0.0		0.0	0.0			0.0	
Total Delay		14.2	4.6	12.1	26.1		48.5	8.8			20.8	
LOS		В	Α	В	С		D	Α			С	
Approach Delay		11.1			25.3			42.5			20.8	
Approach LOS		В			С			D			С	
Queue Length 50th (ft)		102	10	8	242		120	0			1	
Queue Length 95th (ft)		305	63	42	#750		#365	31			12	
Internal Link Dist (ft)		545			749			514			42	
Turn Bay Length (ft)			100	75			50					
Base Capacity (vph)		983	910	381	982		378	468			456	
Starvation Cap Reductn		0	0	0	0		0	0			0	
Spillback Cap Reductn		0	0	0	0		0	0			0	
Storage Cap Reductn		0	0	0	0		0	0			0	
Reduced v/c Ratio		0.48	0.24	0.13	0.84		0.84	0.12			0.01	

Intersection Summary

Cycle Length: 90

Actuated Cycle Length: 71.6

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.84

Intersection Signal Delay: 23.6 Intersection Capacity Utilization 72.5%

Intersection LOS: C

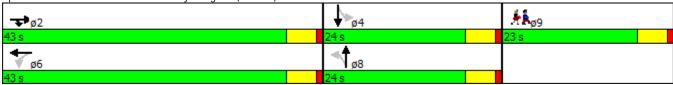
ICU Level of Service C

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 1: Pond St /Driveway & High St (Rte 109)



Synchro 8 Report Page 1

APPENDIX E

MassDOT Highway Division Project Development Process

Overview of the Project Development Process

Transportation decision making is complex and can be influenced by legislative mandates, environmental regulations, financial limitations, agency programmatic commitments, and partnering opportunities. Decision makers and reviewing agencies, when consulted early and often throughout the project development process, can ensure that all participants understand the potential impact these factors can have on project implementation. Project development is the process that takes a transportation improvement from concept through construction.

The MassDOT Highway Division has developed a comprehensive project-development process, which is contained in Chapter 2 of the *MassDOT Highway Division's Project Development and Design Guide*. The eight-step process covers a range of activities extending from identification of a project need, through completion of a set of finished contract plans, to construction of the project. The sequence of decisions made through the project-development process progressively narrows the project focus and, ultimately, leads to a project that addresses the identified needs. The descriptions provided below are focused on the process for a highway project, but the same basic process will need to be followed for non-highway projects as well.

1. Needs Identification

For each of the locations at which an improvement is to be implemented, MassDOT leads an effort to define the problem, establishes project goals and objectives, and defines the scope of the planning needed for implementation. To that end, it has to complete a Project Need Form (PNF), which states in general terms the deficiencies or needs related to the transportation facility or location. The PNF documents the problems and explains why corrective action is needed. For this study, the information defining the need for the project will be drawn primarily, perhaps exclusively, from the present report. Also, at this point in the process, MassDOT meets with potential participants, such as the Metropolitan Planning Organization (MPO) and community members, to allow for an informal review of the project.

The PNF is reviewed by the MassDOT Highway Division district office whose jurisdiction includes the location of the proposed project. MassDOT also sends the PNF to the MPO, for informational purposes. The outcome of this step determines whether the project requires further planning, whether it is already well supported by prior planning studies, and, therefore, whether it is ready to move forward into the design phase, or whether it should be dismissed from further consideration.

2. Planning

This phase will likely not be required for the implementation of the improvements proposed in this planning study, as this planning report should constitute the outcome of this step. However, in general, the purpose of this implementation step is for the project proponent to identify issues, impacts, and approvals that may need to be obtained, so that the subsequent design and permitting processes are understood.

The level of planning needed will vary widely, based on the complexity of the project. Typical tasks include: define the existing context, confirm project need, establish goals and objectives, initiate public outreach, define the project, collect data, develop and analyze alternatives, make recommendations, and provide documentation. Likely outcomes include consensus on the project definition to enable it to move forward into environmental documentation (if needed) and design, or a recommendation to delay the project or dismiss it from further consideration.

3. Project Initiation

At this point in the process, the proponent, MassDOT Highway Division, fills out a Project Initiation Form (PIF) for each improvement, which is reviewed by its Project Review Committee (PRC) and the MPO. The PRC is composed of the Chief Engineer, each District Highway Director, and representatives of the Project Management, Environmental, Planning, Right-of-Way, Traffic, and Bridge departments, and the MassDOT Federal Aid Program Office (FAPO). The PIF documents the project type and description, summarizes the project planning process, identifies likely funding and project management responsibility, and defines a plan for interagency and public participation. First the PRC reviews and evaluates the proposed project based on the MassDOT's statewide priorities and criteria. If the result is positive, MassDOT Highway Division moves the project forward to the design phase and to programming review by the MPO. The PRC may provide a Project Management Plan to define roles and responsibilities for subsequent steps. The MPO review includes project evaluation based on the MPO's regional priorities and criteria. The MPO may assign project evaluation criteria score, a Transportation Improvement Program (TIP) year, a tentative project category, and a tentative funding category.

4. Environmental Permitting, Design, and Right-of-Way Process

This step has four distinct but closely integrated elements: public outreach, environmental documentation and permitting (if required), design, and right-of-way acquisition (if required). The outcome of this step is a fully designed and permitted project ready for construction. However, a project does not have to be fully designed in order for the MPO to program it in the TIP. The sections below provide more detailed information on the four elements of this step of the project development process.

Public Outreach

Continued public outreach in the design and environmental process is essential to maintain public support for the project and to seek meaningful input on the design elements. The public outreach is often in the form of required public hearings, but can also include less formal dialogues with those interested in and affected by a proposed project.

Environmental Documentation and Permitting

The project proponent, in coordination with the Environmental Services section of the MassDOT Highway Division, will be responsible for identifying and complying with all applicable federal, state, and local environmental laws and requirements. This includes determining the appropriate project category for both the Massachusetts Environmental Protection Act (MEPA) and the National Environmental Protection Act (NEPA). Environmental documentation and permitting is often completed in conjunction with the Preliminary Design phase described below.

Design

There are three major phases of design. The first is **Preliminary Design**, which also is referred to as the 25-percent submission. The major components of this phase include full survey of the project area, preparation of base plans, development of basic geometric layout, development of preliminary cost estimates, and submission of a functional design report. Preliminary Design, although not required to be, often is completed in conjunction with the Environmental Documentation and Permitting. The next phase is **Final Design**, which also is referred to as the 75-percent and 100-percent submission. The major components of this phase include preparation of a subsurface exploratory plan (if required), coordination of utility relocations, development of traffic management plans through construction zones, development of final cost estimates, and refinement and finalization of the construction plans. Once Final Design is complete, a full set of **Plans, Specifications, and Estimates (PS&E)** is developed for the project.

Right-of-Way Acquisition

A separate set of Right-of-Way plans are required for any project that requires land acquisition or easements. The plans must identify the existing and proposed layout lines, easements, property lines, names of property owners, and the dimensions and areas of estimated takings and easements.

5. Programming (Identification of Funding)

Programming, which typically begins during the design phase, can actually occur at any time during the process, from planning to design. In this step, which is distinct from project initiation, the proponent requests that the MPO place the project in the region's Transportation Improvement Program (TIP). The proponent requesting the project's listing on the TIP can be the community or it can be one of the MPO member agencies

(the Regional Planning Agency, MassDOT, and the Regional Transit Authority). The MPO then considers the project in terms of state and regional needs, evaluation criteria, and compliance with the regional Transportation Plan and decides whether to place it in the draft TIP for public review and then in the final TIP.

6. Procurement

Following project design and programming of a highway project, the MassDOT Highway Division publishes a request for proposals. It then reviews the bids and awards the contract to the qualified bidder with the lowest bid.

7. Construction

After a construction contract is awarded, MassDOT Highway Division and the contractor develop a public participation plan and a management plan for the construction process.

8. Project Assessment

The purpose of this step is to receive constituents' comments on the project development process and the project's design elements. MassDOT Highway Division can apply what is learned in this process to future projects.

Project Development Schematic Timetable

Step	Schedule Influence	Typical Duration
Step I: Problem/Need/Opportunity Identification The proponent completes a PNF. This form is reviewed by the MassDOT district office, which guides the proponent in subsequent steps of the process.	The PNF may be prepared quickly by the proponent to include any readily available supporting data. The district office will return comments to the proponent within one month of receiving the PNF.	One-to- three months
Step II: Planning Project planning can range from agreeing on a clear solution to a detailed analysis of alternatives and their impacts.	For some projects, no planning beyond preparation of the PNF is required. Some projects require a planning study centered on specific issues associated with a proposed solution or a narrow family of alternatives. Complex projects likely would require a detailed alternatives analysis.	Project Planning Report: three-to- 24+ months
Step III: Project Initiation The proponent prepares and submits a PIF and a TEC form. The MPO and MassDOT district office informally review the PIF and TEC; and the PRC formally reviews them.	The PIF includes refinement of the preliminary information contained in the PNF. Additional information summarizing the results of the planning process, such as the project planning report, is included with the PIF and TEC. The schedule is determined by PRC staff (depending on project complexity) and meeting schedule.	One-to-four months
Step IV: Design, Environmental, and Right-of-Way The proponent completes the project design. Concurrently, the proponent completes necessary environmental permitting analyses and files permit applications. Any right-of-way needed for the project is identified and the acquisition process begins.	The schedule depends upon the size of the project and the complexity of the design, permitting, and right-of-way issues. The MassDOT district and appropriate sections complete the design review.	Three- to- 48+ months
Step V: Programming The MPO considers the project in terms of its regional priorities and determines whether to include the project in the draft TIP, which is made available for public comment, and includes a project description and funding source.	The schedule for this step is subject to each MPO's programming cycle and meeting schedule. It is possible that the MPO will not include a project in its draft TIP based on its review and approval procedures.	Three-to- 12+ months

Step	Schedule Influence	Typical Duration
Step VI: Procurement The project is advertised for construction and a contract is awarded.	Administration of competing projects can influence the advertising schedule.	One-to-12 months
Step VII: Construction The construction process is initiated including public notification and any anticipated public involvement. Construction continues to project completion.	The duration of this step is entirely dependent upon project complexity and phasing.	Three-to- 60+ months
Step VIII: Project Assessment The construction period is complete and project elements and processes are evaluated on a voluntary basis.	The duration of this step is dependent upon the proponent's approach and any required follow-up.	One month

Source: MassDOT Highway Division Project Development and Design Guide.